

## ***What is Convective Parameterization?***

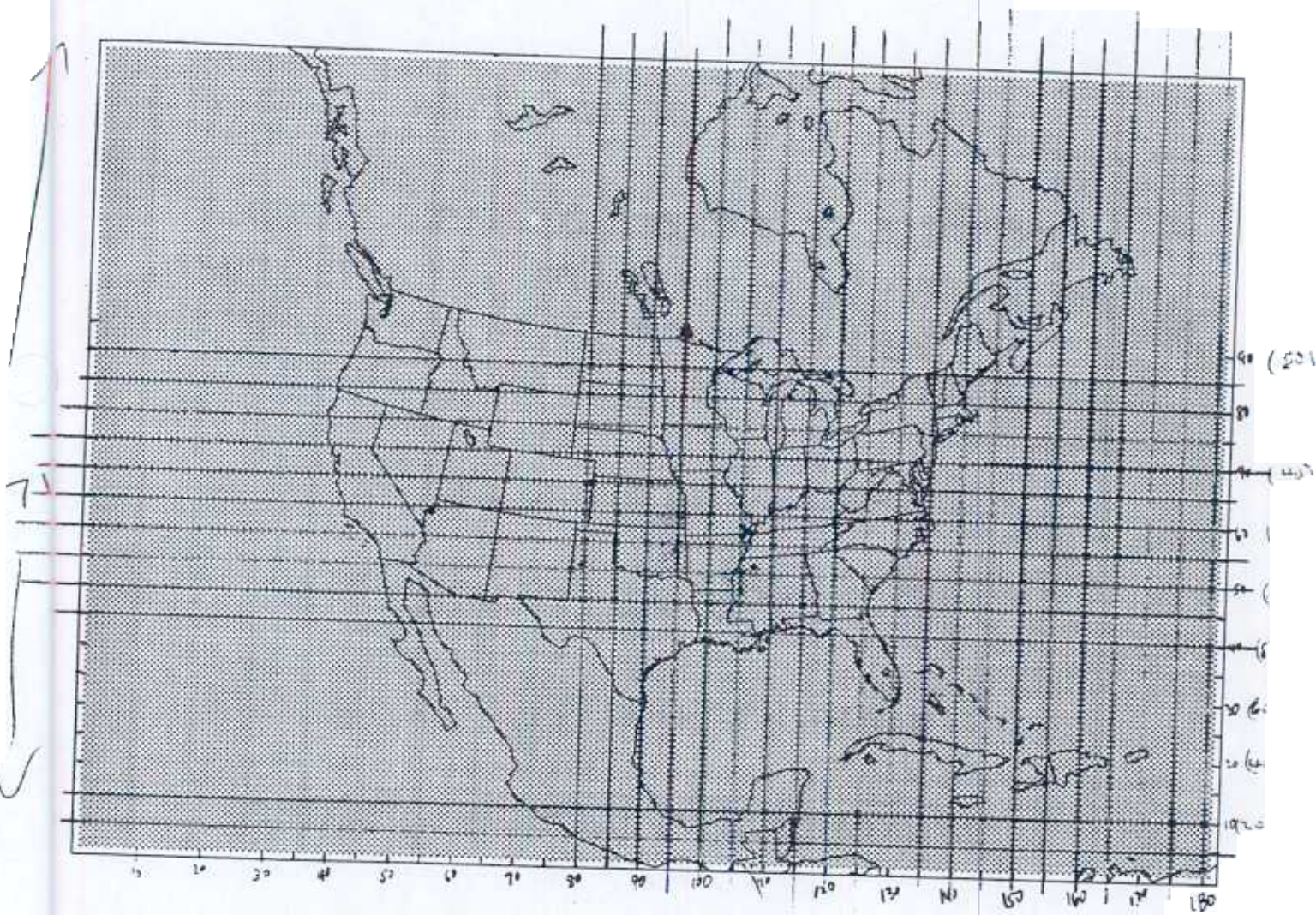
*A technique used in NWP to predict the collective effects of (many) convective clouds that may exist within a single grid element*





# ETA GRID H POINTS

$$\begin{matrix} I=127 \\ T=30 \end{matrix}$$



← 181 (max) →

I

$$\begin{matrix} I=54 \\ T=108 \end{matrix}$$

$$\begin{matrix} I=93 \\ T=120 \end{matrix}$$

$$\begin{matrix} I=106 \\ T=115 \end{matrix}$$

$$\begin{matrix} I=115 \\ T=110 \end{matrix}$$

$$\begin{matrix} I=80 \\ T=124 \end{matrix}$$

$$\begin{matrix} I=102 \\ T=117 \end{matrix}$$

106

## ***Why do NWP models need to worry about it?***

- ***Direct Concern: To predict convective precipitation***
- ***Feedback to Larger Scales: Deep convection "overturms" the atmosphere, strongly affecting mesoscale and larger scale dynamics:***

*Changes vertical stability*

- *redistributes and generates heat*
- *redistributes and removes moisture*
- *Makes clouds, strongly affecting surface heating and atmospheric radiation*



## *How Does the Feedback Occur in a Model?*

*...At every model grid point, predictive variables change each time step as a function of a number of processes, including convection...*

*temperature*

$$\frac{d\theta}{dt} = P_{\text{rad}} + P_{\text{conv}} + P_{\text{cond/evap}} + P_{\text{hdiff}} + P_{\text{vdiff}} + P_{\text{sfc}}$$

*where*

$$\frac{d\theta}{dt} = \frac{\partial\theta}{\partial t} + u \frac{\partial\theta}{\partial x} + v \frac{\partial\theta}{\partial y} + \omega \frac{\partial\theta}{\partial p}$$

*water vapor*

$$\frac{dq_v}{dt} = + P_{\text{conv}} + P_{\text{cond/evap}} + P_{\text{hdiff}} + P_{\text{vdiff}} + P_{\text{sfc}}$$

*u (and v)-momentum*

$$\frac{du}{dt} + \frac{1}{\rho} \frac{\partial p}{\partial x} - f_v = (\mathbf{P}_{\text{conv}}) + \mathbf{P}_{\text{hdiff}} + \mathbf{P}_{\text{vdiff}} + \mathbf{P}_{\text{sfc}}$$

*...When activated, a convective parameterization computes the changes in Temperature and Moisture (possibly cloud water, momentum, etc.) that would occur at each vertical level if convection developed in the given grid-point environment...*

*for example,*

$$\left. \frac{\partial \theta}{\partial t} \right|_{\text{conv}} = \frac{\theta_{\text{final}} - \theta_{\text{initial}}}{\tau_c} = \mathbf{P}_{\text{conv}}$$

*where  $\tau_c$  is a convective time scale, typically 30 mins. to 1 hr.*

## ***How to Parameterize...***

- Relate unresolved effects (convection) to grid-scale properties using statistical or empirical techniques
- What properties of convection do we need to predict?
  - *convective triggering* **(YES/NO)**
  - *convective intensity (how much rainfall/heating?)*
  - *vertical distribution of heating*
  - *vertical distribution of drying*



## *When, Where, and How much...*

- *Triggering (always requires positive area on a thermodynamic [e.g., Skew-T, Log-P] diagram)*

Different approaches; **either**

- *Mass or moisture convergence threshold exceeded at a grid point, or*
- *Positive destabilization rate, or*
- *Perturbed parcels can reach their level of free convection*

**- CLOUD-LAYER MOISTURE IS SUFFICIENT**

- *Convective Intensity (net heating)*

*either*

- *Proportional to mass or moisture convergence, or*
- *Sufficient to offset large-scale destabilization rate,*  
*or*

✓ - *Sufficient to eliminate CAPE (CONSTRAINED BY AVAILABLE MOISTURE)*

- ***Vertical distribution of heating and drying***

*either*

*determined by nudging to empirical reference profiles, or*

*- estimated using a simple 1-d cloud model to satisfy the constraints on intensity*

**Schemes based on mass, moisture convergence  
(e.g., Kuo-type schemes)**

**IF:**

- 1.) Atmosphere is conditionally unstable;
- 2.) Horizontal moisture (or maybe mass) convergence is positive

**THEN:**

- 3.) Converged moisture is assumed to go up in deep convective clouds (rather than broadscale ascent)
- 4.) Convective heating is distributed vertically according to the distribution of  $T' - T$ , where  $T'$  is the temperature on the moist adiabat of most-unstable air.
- 5.) Moisture is all condensed out (or a specified fraction is condensed out).

## **Quasi-Equilibrium Schemes (i.e., Arakawa-Schubert)**

- Large-Scale destabilization rate  $\approx$  Convective Stabilization Rate
- Convective Stabilization is Achieved by an Ensemble of Clouds



*Current EMC Operational Models all use  
Different Approaches to Convective  
Parameterization...*

**RUC II:** *Grell scheme\**

**Eta:** *Betts-Miller-Janjic scheme\**  
*(Kain-Fritsch\* used on an experimental  
basis)*

**MRF/AVN:** *Grell-Pan scheme\**

*\*The Grell, Grell-Pan, and Kain-Fritsch schemes  
are Mass-Flux schemes, meaning that they use  
simple cloud models to simulate rearrangements of  
mass in a vertical column.*

*\*The Betts-Miller-Janjic scheme adjusts to "mean  
post-convective profiles" based on widespread  
observations.*

# Grell and Grell-Pan Schemes: (basic operating principles)

## 1.) Initiation (on/off switch)

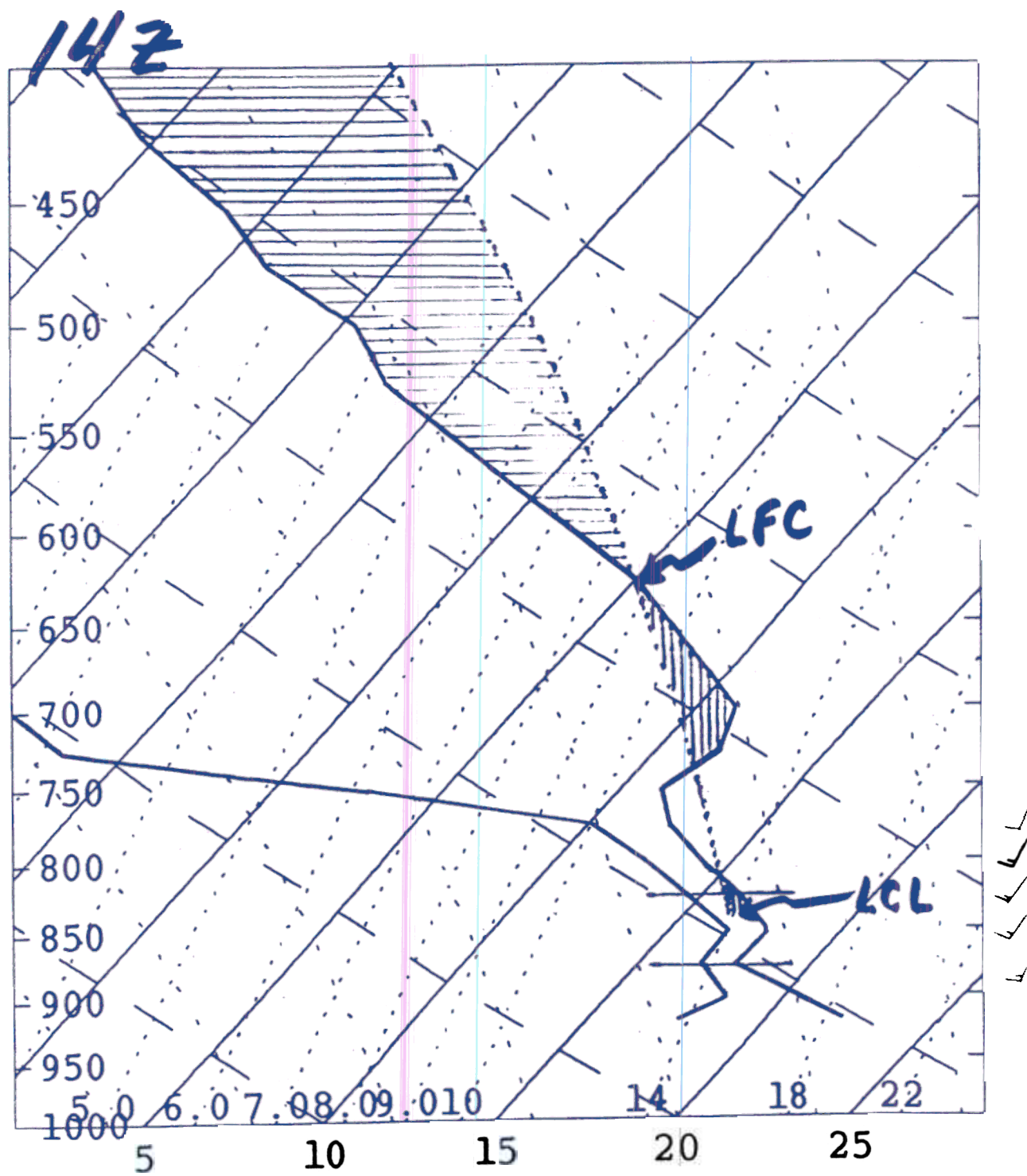
- Find highest  $\theta_e$  air in column below  $\sim 400$  mb level...does CAPE exist for this air?
- Is CAP too strong? How far does parcel have to be lifted to reach LFC?  
Is  $P(\text{source}) - P(\text{LFC})$  less than 150 mb?

Is large-scale destabilization rate positive?  
*i.e.*, is  $d(\text{CAPE})/dt > 0$ ?

If yes to all 3, initiate convection..

## 2.) Characteristics of Convection

- use simple models of an updraft and downdraft to simulate mass rearrangements by convection
- make updraft and downdraft mass fluxes strong enough that their stabilizing effect approximately balances rate of large-scale destabilization:



# Grell and Grell-Pan Schemes: (basic operating principles) (cont.)

$$\left[ \frac{d(\text{CAPE})}{dt} \right]_{\text{convection}} \approx - \left[ \frac{d(\text{CAPE})}{dt} \right]_{\text{large-scale}}$$

## 3.) Feeding back the effects of convection

- Introduce tendency terms in the prognostic equations for temperature and moisture:

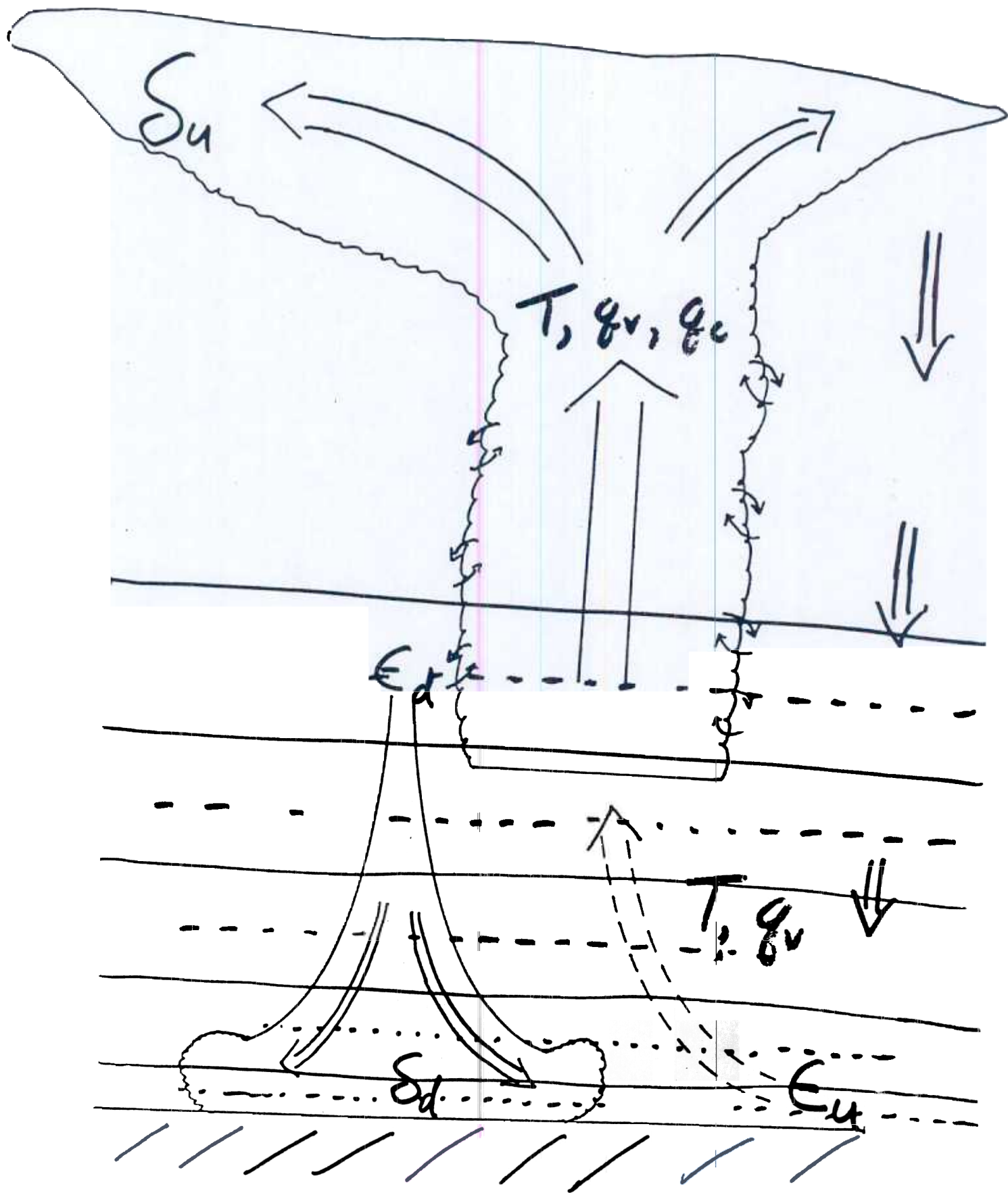
$$\left. \frac{\partial \alpha}{\partial t} \right|_{\text{conv}} = \frac{\alpha_{\text{final}} - \alpha_{\text{initial}}}{\tau_c},$$

where  $\alpha$  represents  $T$  or  $q_v$

## Kain-Fritsch Scheme...

basic operating principles are similar to Grell-type schemes, except...

- Convective inhibition evaluated in terms of negative area, not just pressure depth
- Large-scale destabilization not required, only CAPE
- Updraft and downdraft formulations more sophisticated
- Convective intensity based on instantaneous CAPE value rather than  $d(\text{CAPE})/dt$





## Kain-Fritsch convective initiation check

- Beginning at the surface, mix in model layers overhead until a mixture 50-100 mb deep is found. This comprises a potential updraft source layer. Find mean  $\theta$ ,  $q_v$  of this layer.
- Lift a parcel with these characteristics to its LCL. At the LCL, Compute a temperature perturbation,  $\Delta T_p$  based on grid-point vertical velocity:

$$> \Delta T_p = (w_g - w_c)^{1/3} + \Delta T_p(RH)$$

where  $w_g$  is the grid point vertical velocity (cm/s)  
 $w_c$  is a correction factor:

$$w_c = 2. * Z(LCL)/2 \text{ km}$$

For Example:

|                                    |                                    |
|------------------------------------|------------------------------------|
| $\frac{w_g - w_c}{1 \text{ cm/s}}$ | $\frac{\Delta T_p}{1.0 \text{ K}}$ |
| >>>                                | >>>                                |
| 10 cm/s                            | 2.15 K                             |

In the Eta model, an additional perturbation,  $\Delta T_p(RH)$ , of magnitude  $\sim 0.5 \text{ K}$  is given to account for low RHs in the model

*So...In a typical convective environment with some larger-scale forcing,  $\Delta T_p \sim 1 - 2 \text{ K}$*

## Kain-Fritsch convective initiation check

(cont.)

- Is  $(T_p(\text{LCL}) + \Delta T_p) > T_g$  ???
  - > If no, move up one model level and repeat the process above
- If yes, then compute a vertical velocity perturbation,  $W_p$ , based on magnitude of  $\Delta T_p$ .  
For  $\Delta T_p = 1.5\text{K}$ ,  $W_p \approx 4 - 5 \text{ m/s}$
- Release a parcel at the LCL with temperature given by  $T_p(\text{LCL})$  and vertical velocity given by  $W_p$ , begin solving "parcel buoyancy equation" at sequential model levels overhead
- Determine cloud top as the highest model level at which  $W_p > 0$ .
- Is  $Z(\text{top}) - Z(\text{LCL}) > 3 \text{ km}$ ?
  - > If yes, initiate deep convection from this source layer
  - > If no, remember this layer as a possible source for shallow convection, move up to next potential source layer and repeat all above steps.
- If no potential source layer in lowest 300 mb can generate a convective cloud, move on to the next grid point...

## *The stabilizing mechanisms of the Kain-Fritsch scheme*

- Convective Updraft

- > Removes high  $\theta_e$  air from lower troposphere, transports it aloft.
- > Generates condensation

- Convective Downdraft

- > Draws mass from layer beginning at cloud base and extending up 150 - 200 mb.
- > Deposits low  $\theta_e$  air in subcloud layer
- > Assumed to be saturated above cloud base, RH decreasing at  $\sim 10\%/km$  below cloud base.
- > Continues until it either 1.) reaches the surface, or 2.) becomes warmer than the environment.
- > Mass flux  $\approx$  updraft mass flux at cloud base.

- Return flow, i.e., "compensating subsidence"

- > Compensates for any mass surplus or deficit created by Updraft and Downdraft...Typically, the updraft creates a mass surplus aloft and deficit below so that this return flow is downward

*KF Scheme: How much precip is generated?*

*It depends...*

- > Updraft generates condensate*
- > Updraft dumps condensate into environment*
- > Downdraft evaporates condensate at a rate that depends on:*
  - RH of downdraft source air*
  - Depth of downdraft*
- > Leftover condensate accumulates at surface as Precipitation*

*KF scheme: How does it affect resolved flow?*

*> Heating, Drying, and precipitation tendencies are fed back to resolved-scale equations over a time period of 30 mins to 1 hour.*

## Betts-Miller scheme: (basic operating principles)

- Checks for CAPE - highest  $\theta_e$  air in the lowest ~~500~~<sup>130</sup>mb
- makes a first guess at an "adjusted" temperature profile based on a moist adiabat
- makes a corresponding first guess at a reference *moisture* profile, based on an imposed *subs*aturation ( $\sim$  relative humidity)

imposes enthalpy conservation:

$$\int_{\text{sfc}}^{\text{top}} L_v dq_v = \int_{\text{sfc}}^{\text{top}} C_p dT$$

This usually requires an adjustment ("sliding over" on a skew-T) of both temperature and moisture.

### *Implications of this adjustment:*

- *Betts convection will be weak (or non-existent) when column-mean relative humidity is low even if CAPE is present, will increase in intensity as column moistens.*

- Nudges grid-scale T,  $q_v$  to convectively adjusted values over a specified time period ( $\sim$  1 hour)



## Equilibrium assumption

Convective precipitation acts to move a convectively unstable atmosphere toward some equilibrium state (such as a moist adiabatic lapse rate)

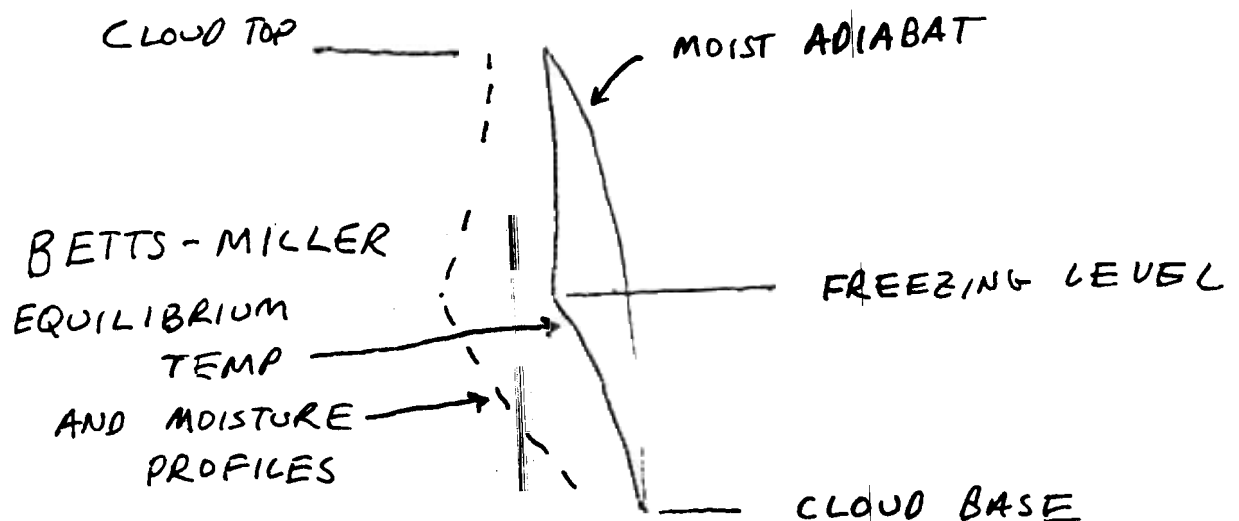
Different schemes define the 'equilibrium state' in different ways

- moist adiabatic
- modification of a moist adiabatic
- results from a cloud model

# Convective - equilibrium type

## Betts-Miller scheme

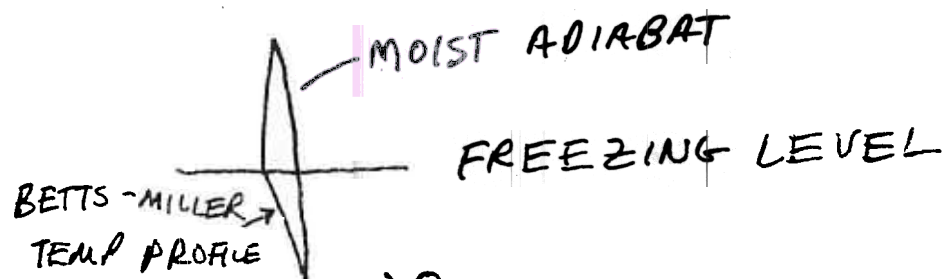
the equilibrium profile is a modified moist adiabat



moisture profile is determined by saturation point deficits (DSP's)

# How the equilibrium (reference) profile is computed.

## Temperature



slope of profile is  $0.85 \frac{\partial \theta_e}{\partial p}$  below the freezing level

profile is connected to original  $\theta_e$  at cloud top, making it more stable than a moist adiabat above freezing level

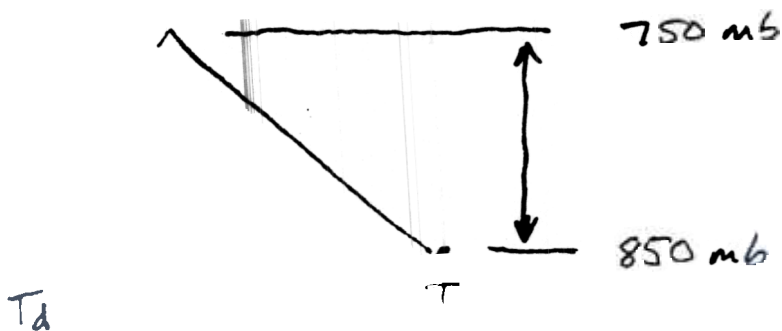
## profiles based upon observational evidence

**Saturation point deficit (DSP) is similar to dewpoint depression**

**It is the pressure change that a parcel must undergo in adiabatic expansion to reach saturation**

**For example**

**a parcel at 850 mb with a temperature of  $10^{\circ}\text{C}$  and a RH of 60%**



**would have a DSP of -100 mb**

# Moisture

critical DSP's are specified

|                           |       |                         |
|---------------------------|-------|-------------------------|
| cloud <del>base</del> TOP | -22.5 | TYPICAL<br>RH<br>40-50% |
| freezing level            | -70.5 | 60-70%                  |
| cloud <del>top</del> BASE | -48.5 | ~80%                    |

different sets are used over  
land and sea

## land

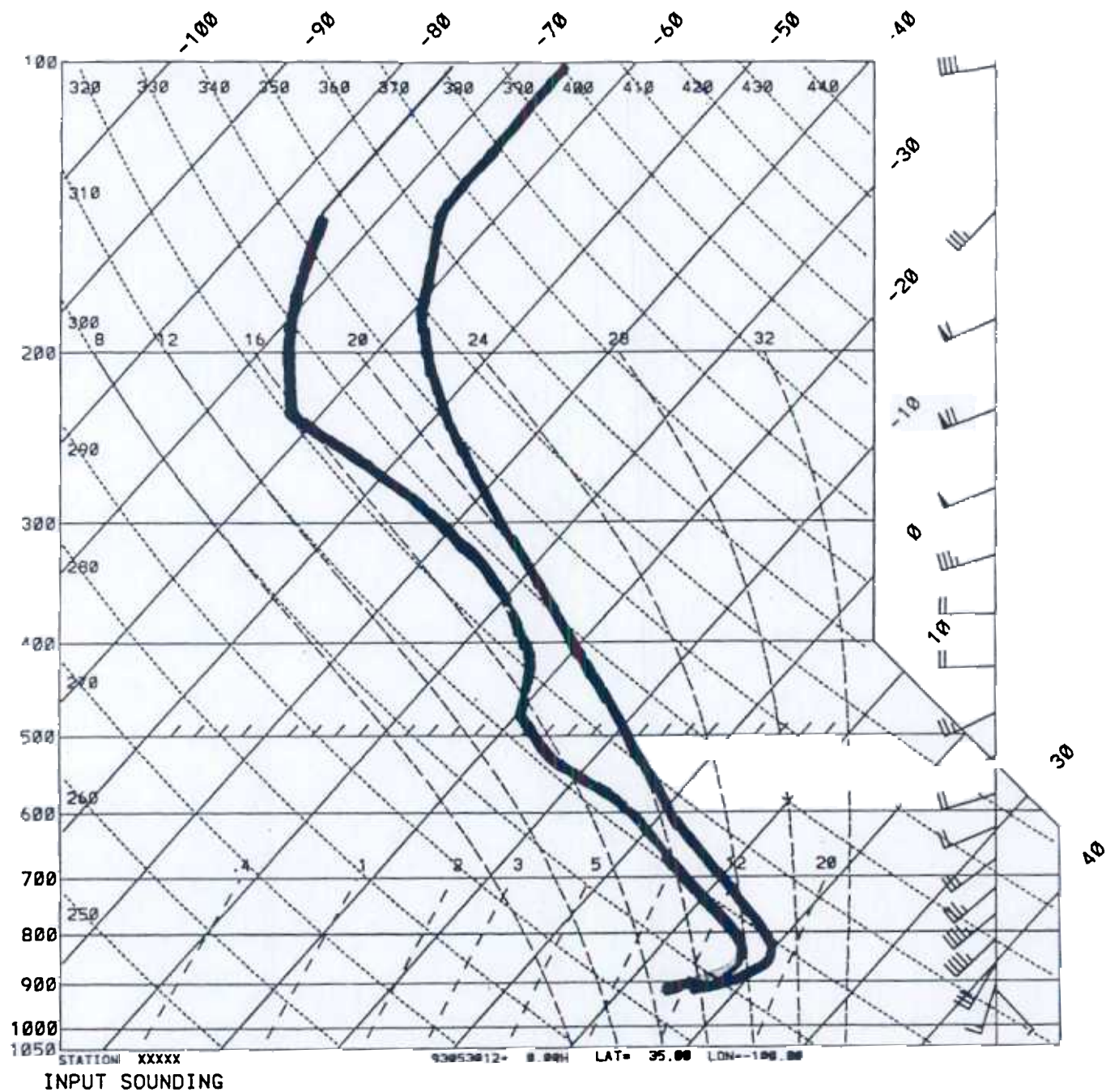
*drier (larger)*  
easier to  
to produce  
precipitation

## sea

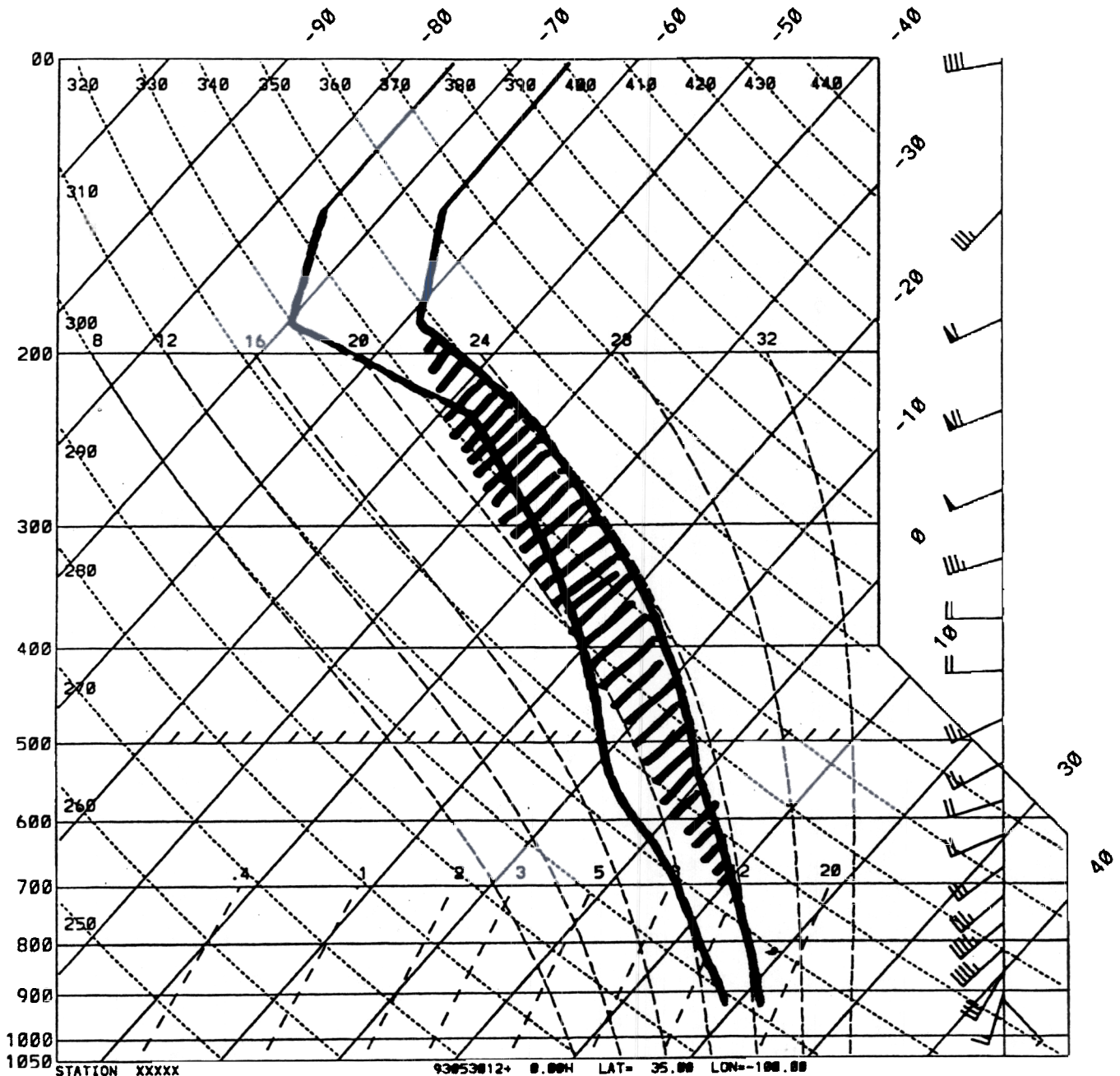
*moister (smaller)*  
more difficult  
to produce  
precipitation

these are modified by "cloud-efficiency" as well





# BETTS



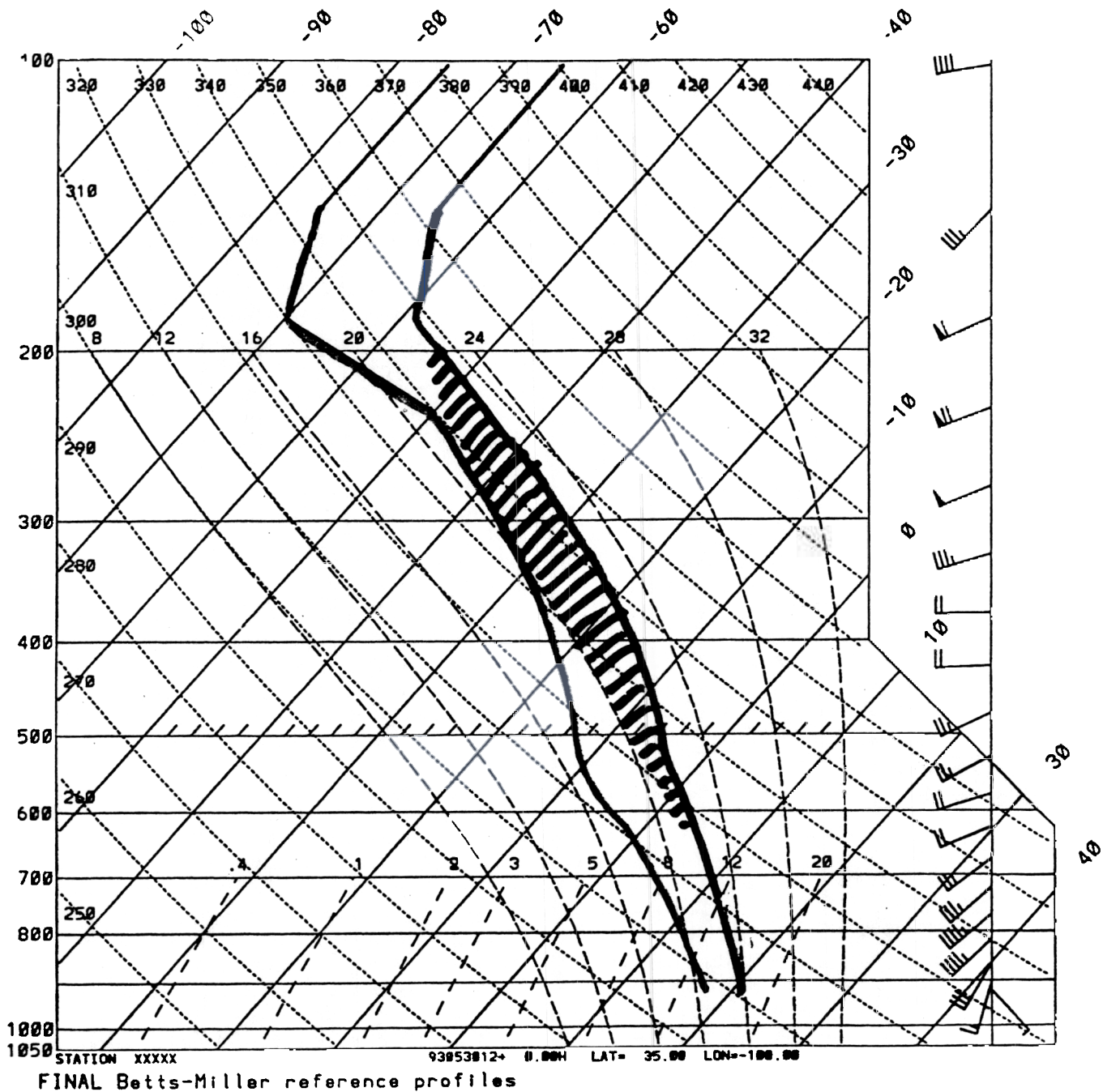
FIRST-GUESS Betts-Miller reference profiles

FIRST-GUESS ADJUSTED PROFILE

— T  
— Sv



# BETTS



FINAL ADJUSTED PROFILE

—T  
—8v

## STEP #1

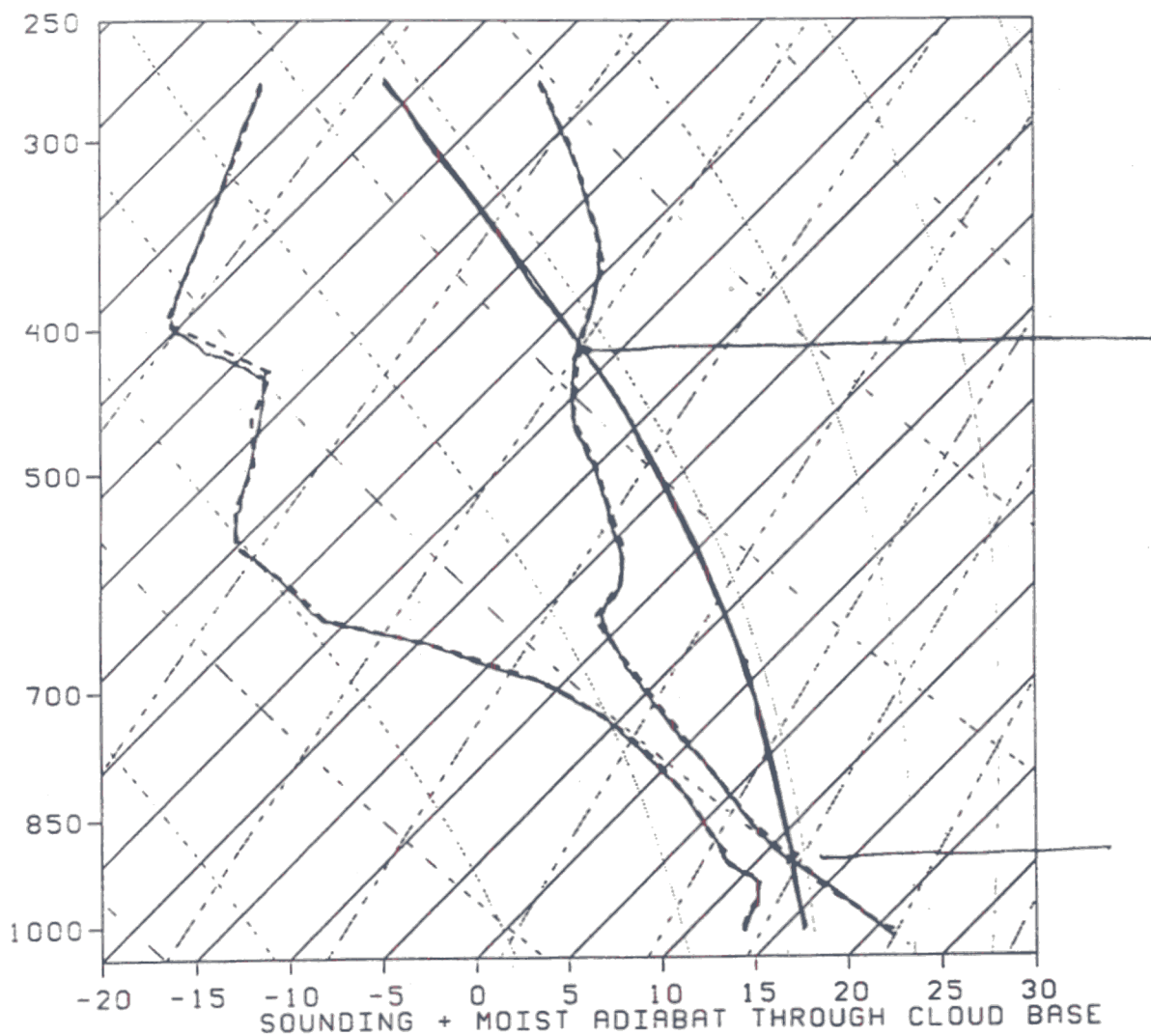
### Determine Cloud Depth

IF  $> 290$  mb  $\rightarrow$  DEEP CONVECTION

IF  $< 290$  mb  $\rightarrow$  SHALLOW  $\therefore$  NO PRECIP

980422/2200 11111 05M

chs22



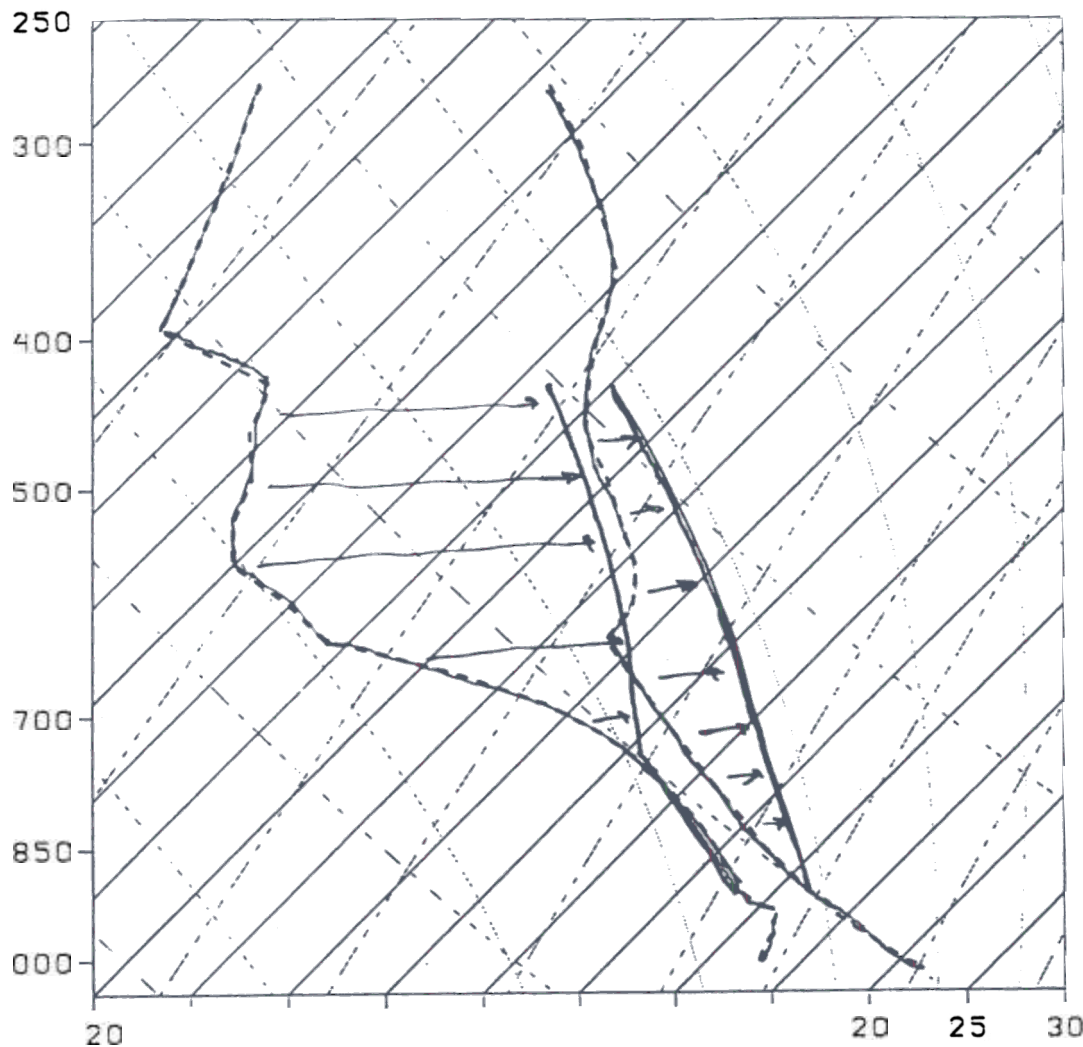
1. Find most unstable parcel in lowest 130 mb above ground.
2. Find LCL of that parcel = CLOUD BASE.

# STEP #2

## Compare Reference Profiles

980422 2200 22

048  
INST GUE DEEP PROFIL



almost  
a  
 $\Delta T, q$   
 $> 0$

does NOT  
make  
physical  
sense!

Temp profile - starts at  $T(\text{mode})$  at  
cloud base goes slightly more unstable  
than moist adiabat up to 0°C level,  
then connects to original moist adiabat + cloud  
top

2 q profile prescribed DSP profile

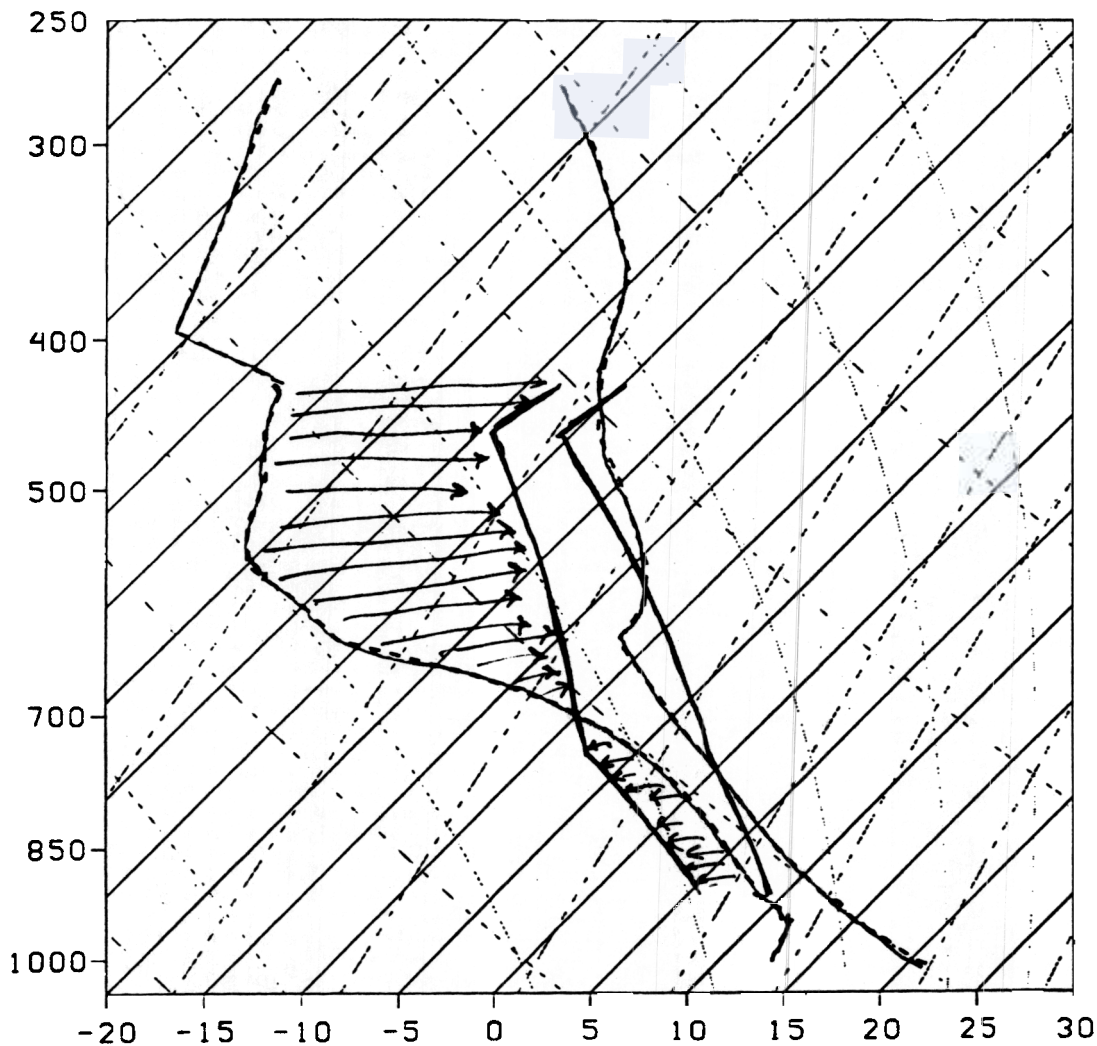
### STEP #3

Adjust Reference profiles  
to total enthalpy

$$\sum [C_p \Delta T + L \Delta q] \Delta p = 0$$

980422/2200 33333

due  
convection



too  
dry  
aloft

### STEP #4

$$\text{Compute precip} = [\Delta q] \frac{\Delta p}{g}$$

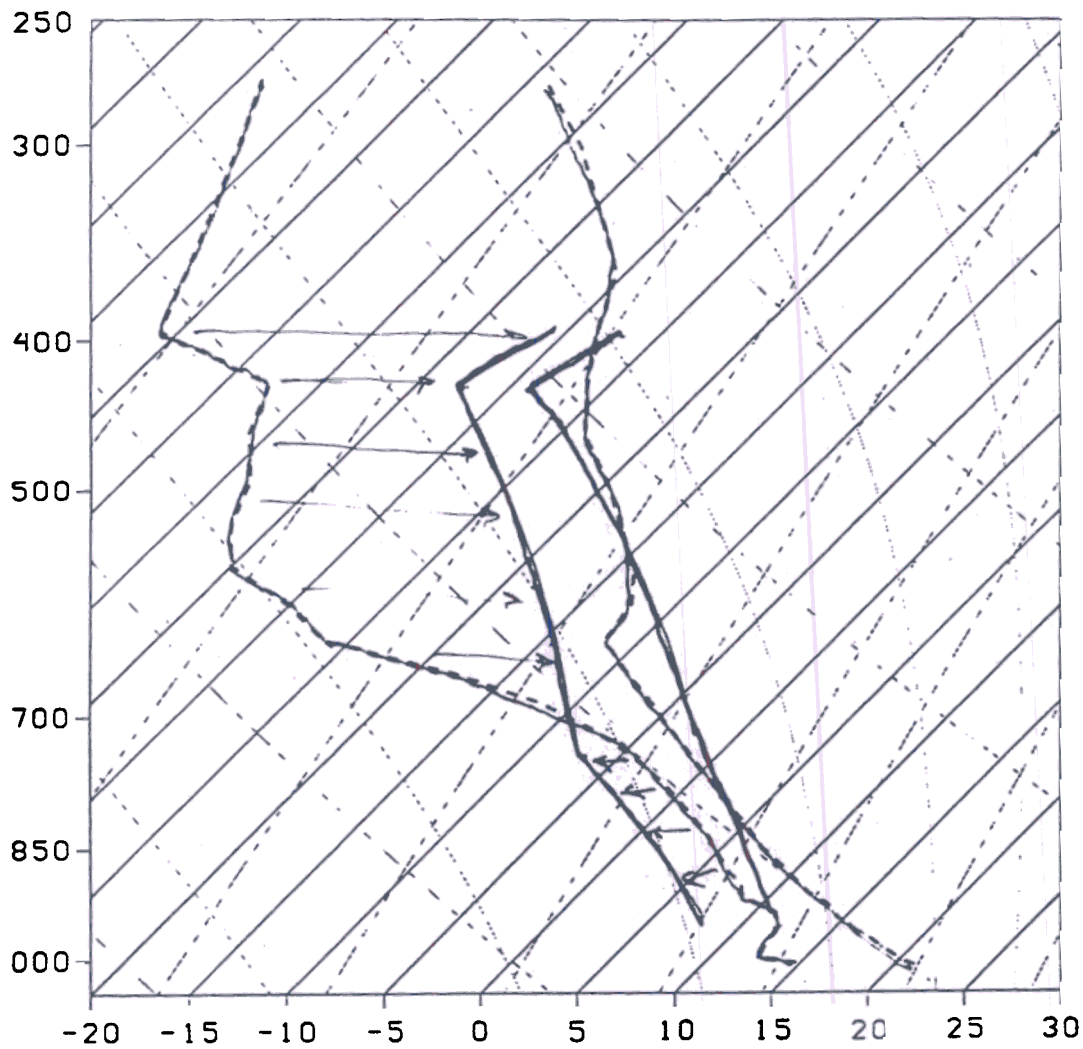
if  $> 0$  SUCCESS!

if  $\leq 0$  goto SHALLOW  $\therefore$  no precip



... After enthalpy adjustment  
ended up right back  
as we started

S80422/2200 33333 GRB chslow  
ADJUSTED DEEP PROFILE



TOO  
DRY

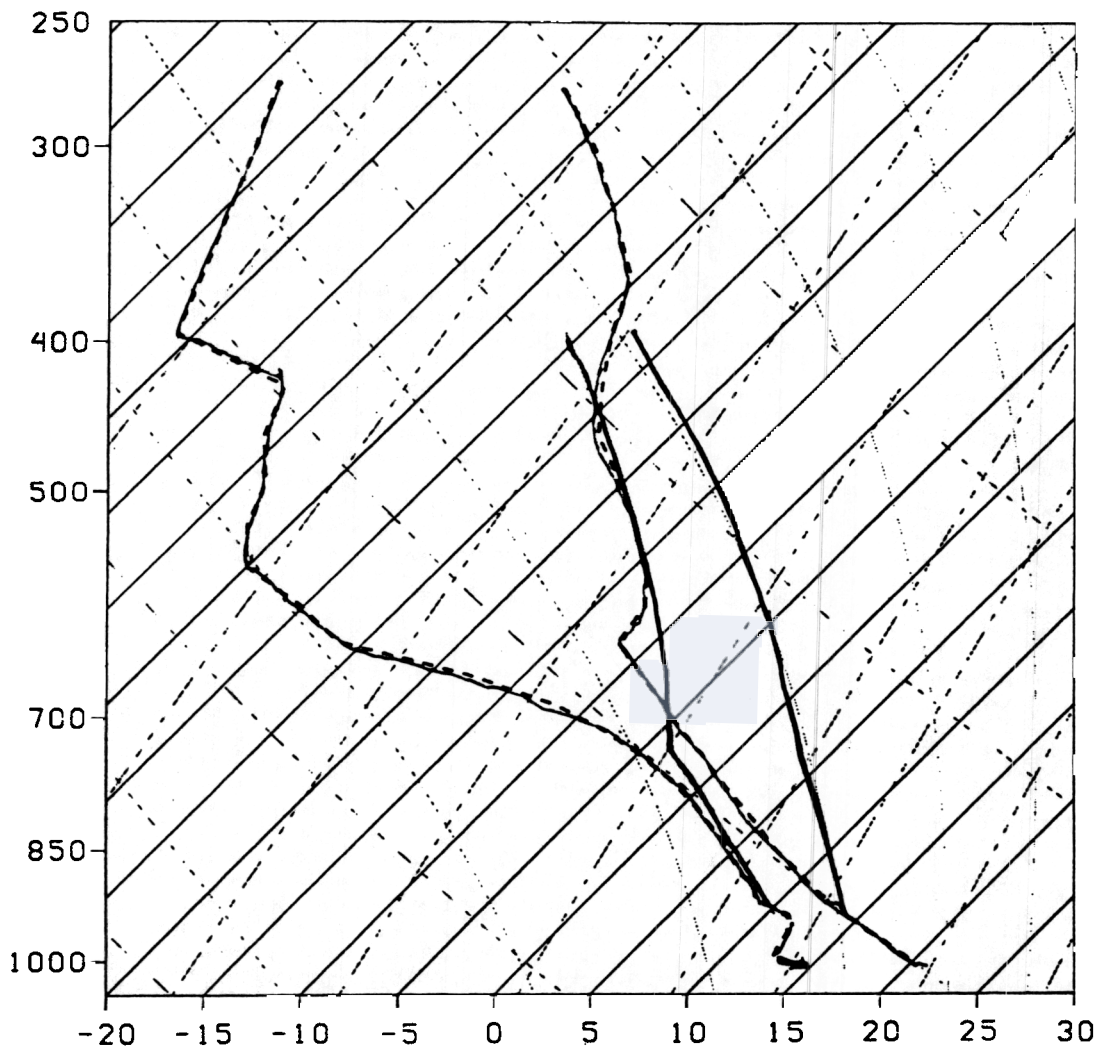
NO  
PRECIP

Modified sounding

Add  $2^\circ$  to low level

$T_d$

980422/2200 22222 OBS CHSLOW  
FIRST GUESS DEEP PROFILE



more  
CAPE

still  
too  
dry  
will  
require

larger  
enthalpy  
adjustment



Modified sounding

increase moisture

between 400 - 600 mb

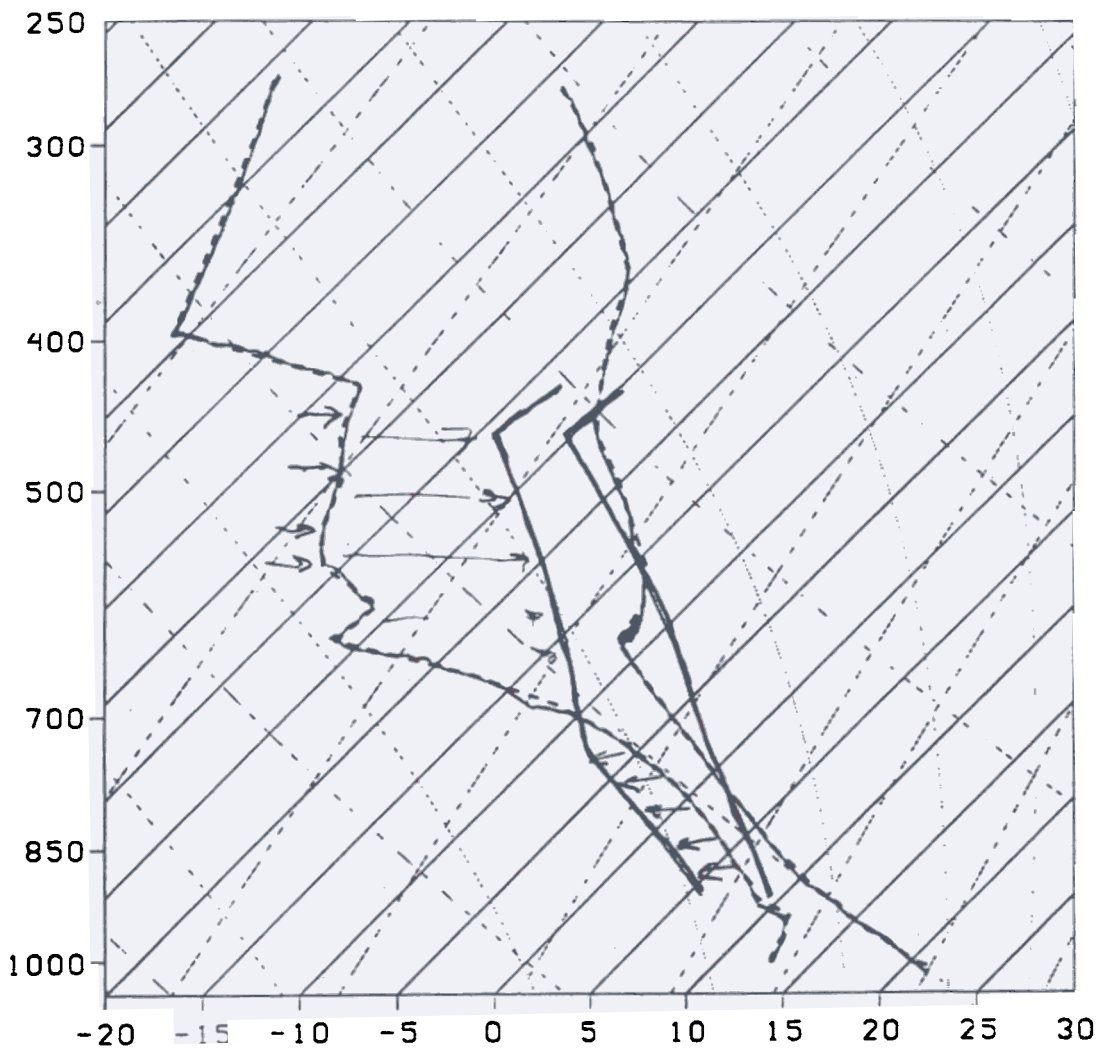
(by about  $3^{\circ}$  Td)

980422/2200 33333

GRB

CHSUPW

ADJUSTED DEEP PROFILE

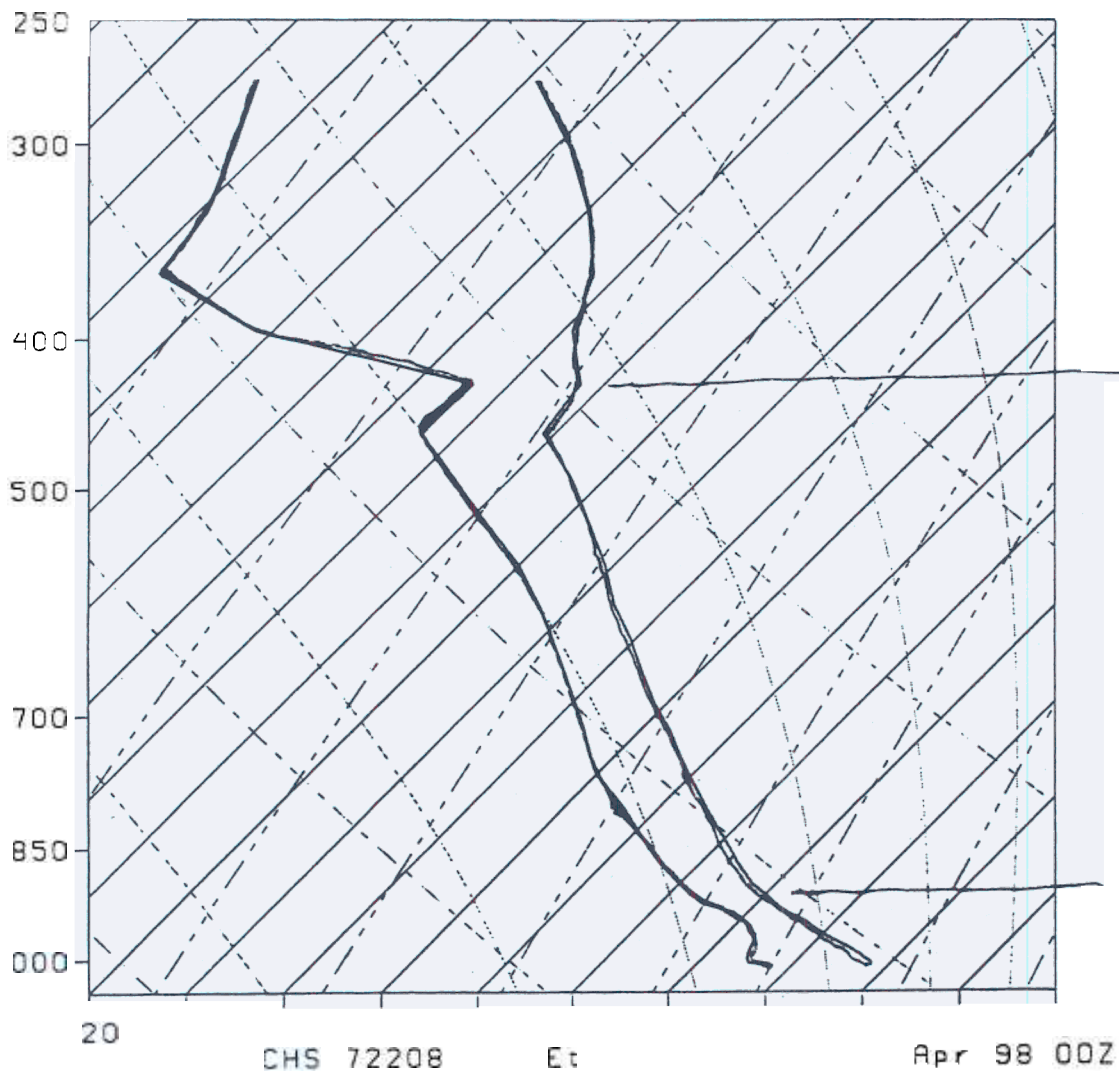


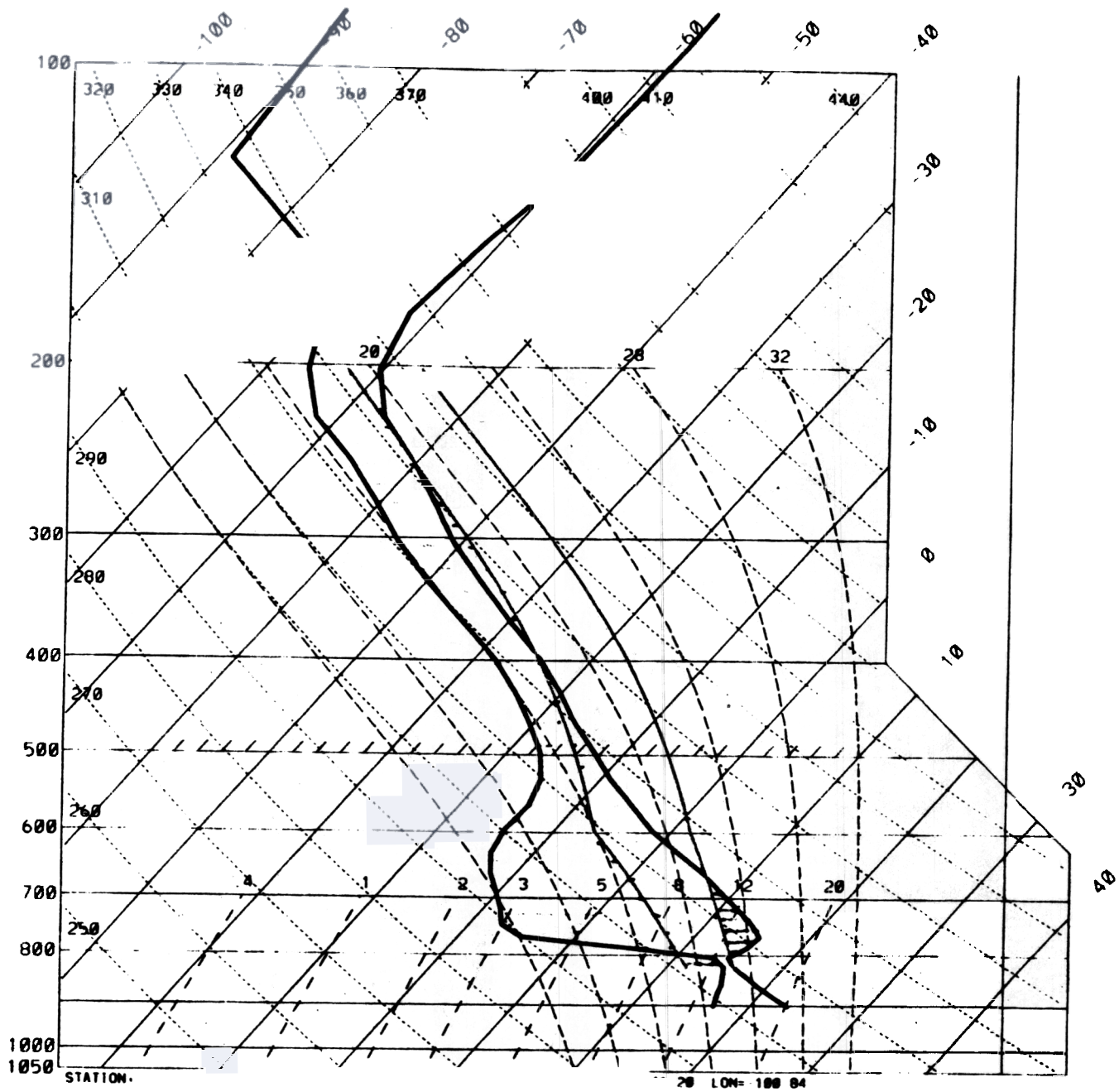
NOW  
THERE  
IS  
ENOUGH  
MOISTURE  
TO  
PRODUCE  
PRECIP

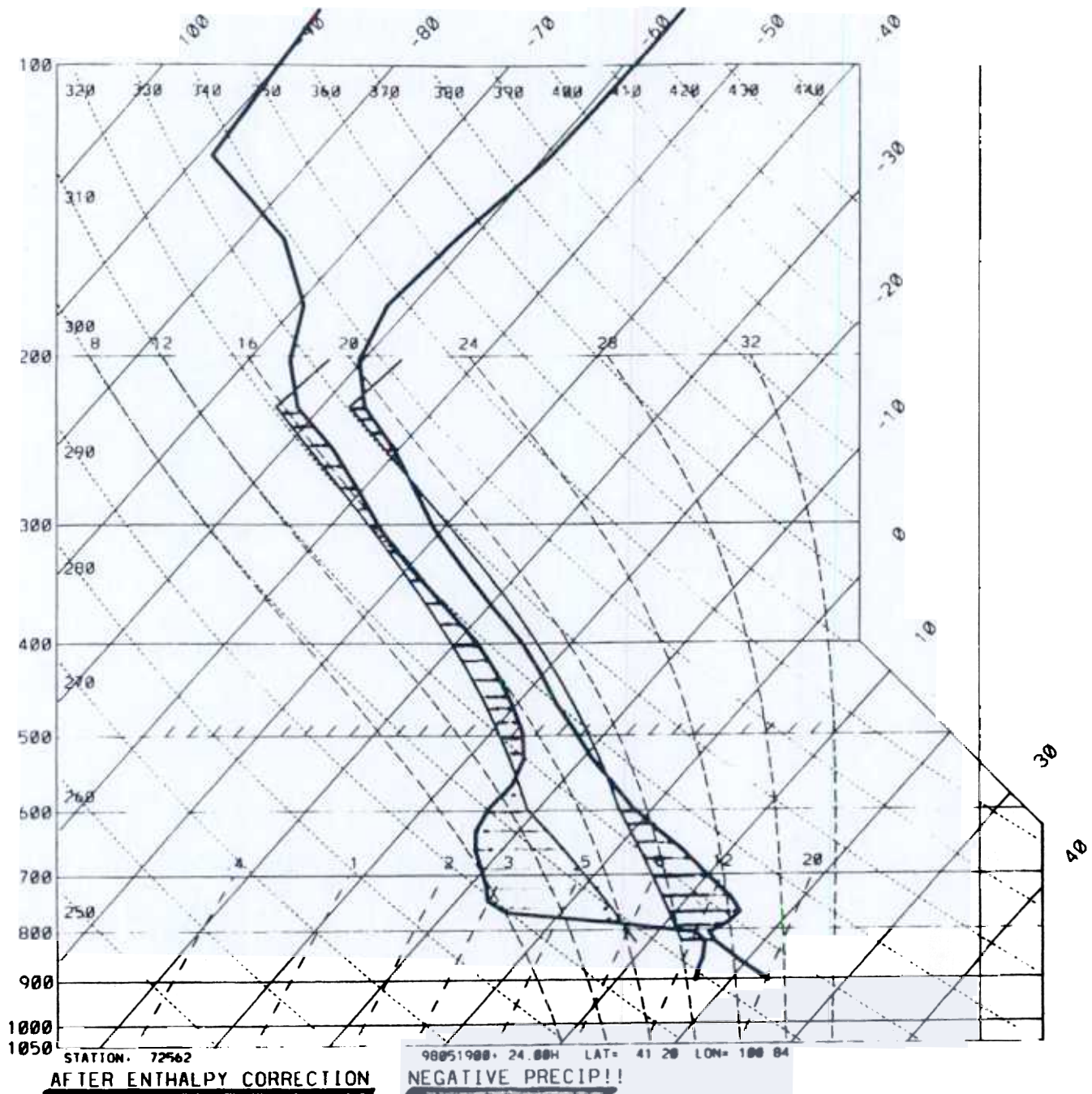
CHS 2 hours later

convection has broken out  
in the model

930423 0000 2208



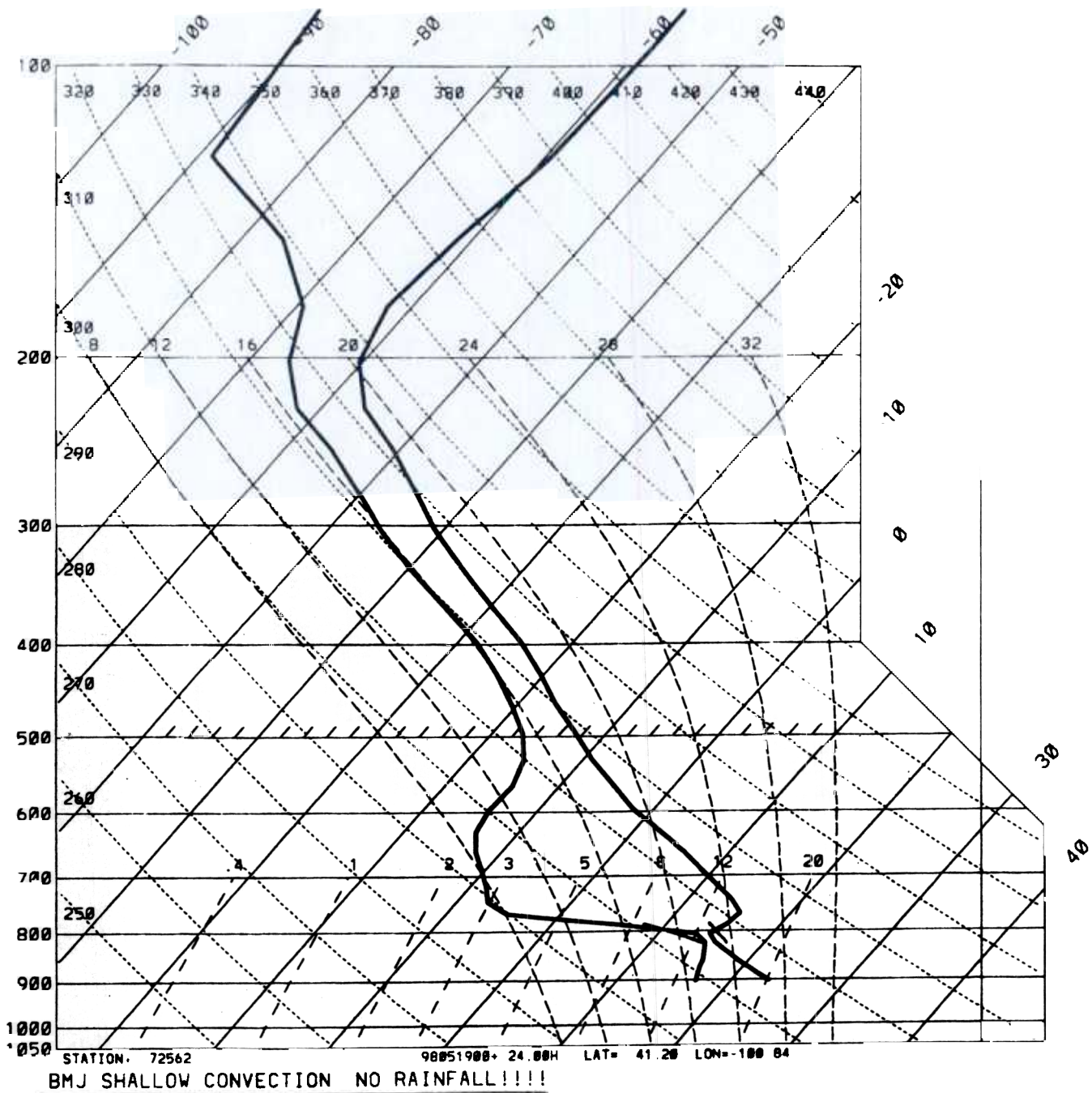




NEGATIVE PRECIP:  $\sum_{\text{BOTTOM}}^{\text{TOP}} \delta q_v > 0$

$\sum_{\text{BOTTOM}}^{\text{TOP}} \delta T < 0$

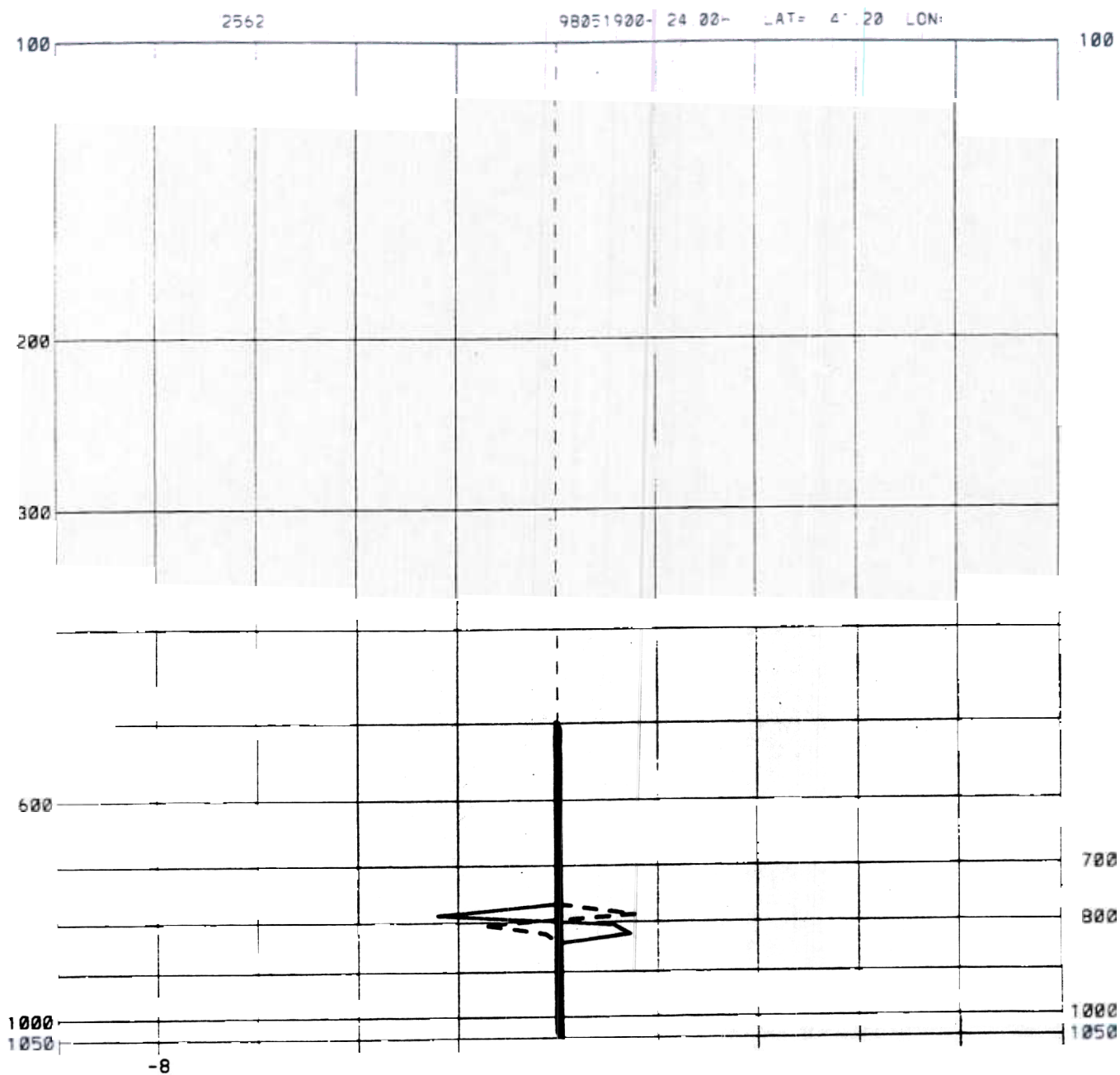




ALLOW ONLY SHALLOW  
CONVECTION:

$$\sum_{\text{BOTTOM}}^{\text{TOP}} \delta q_v = 0$$

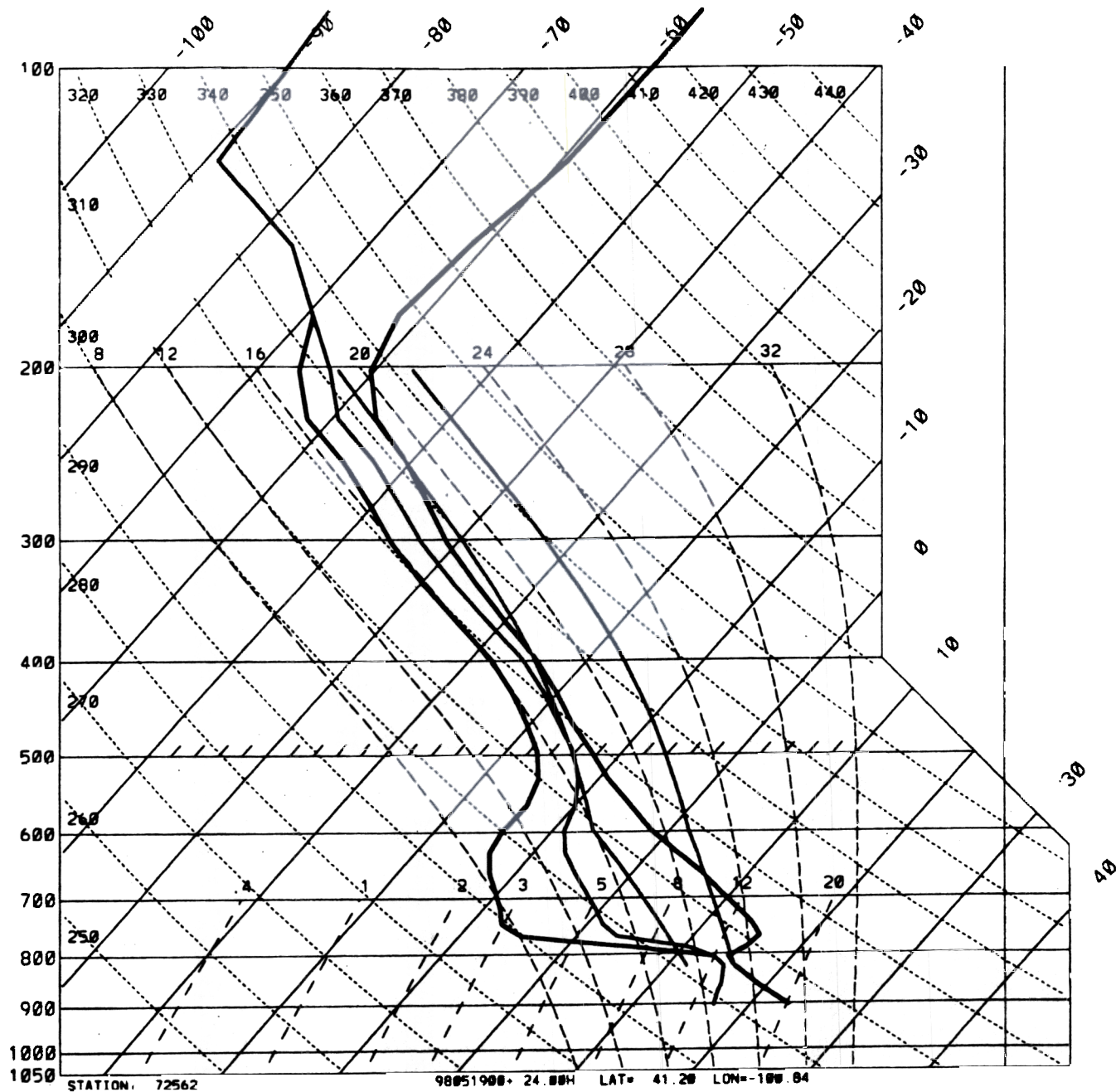
$$\sum_{\text{BOTTOM}}^{\text{TOP}} \delta T = 0$$

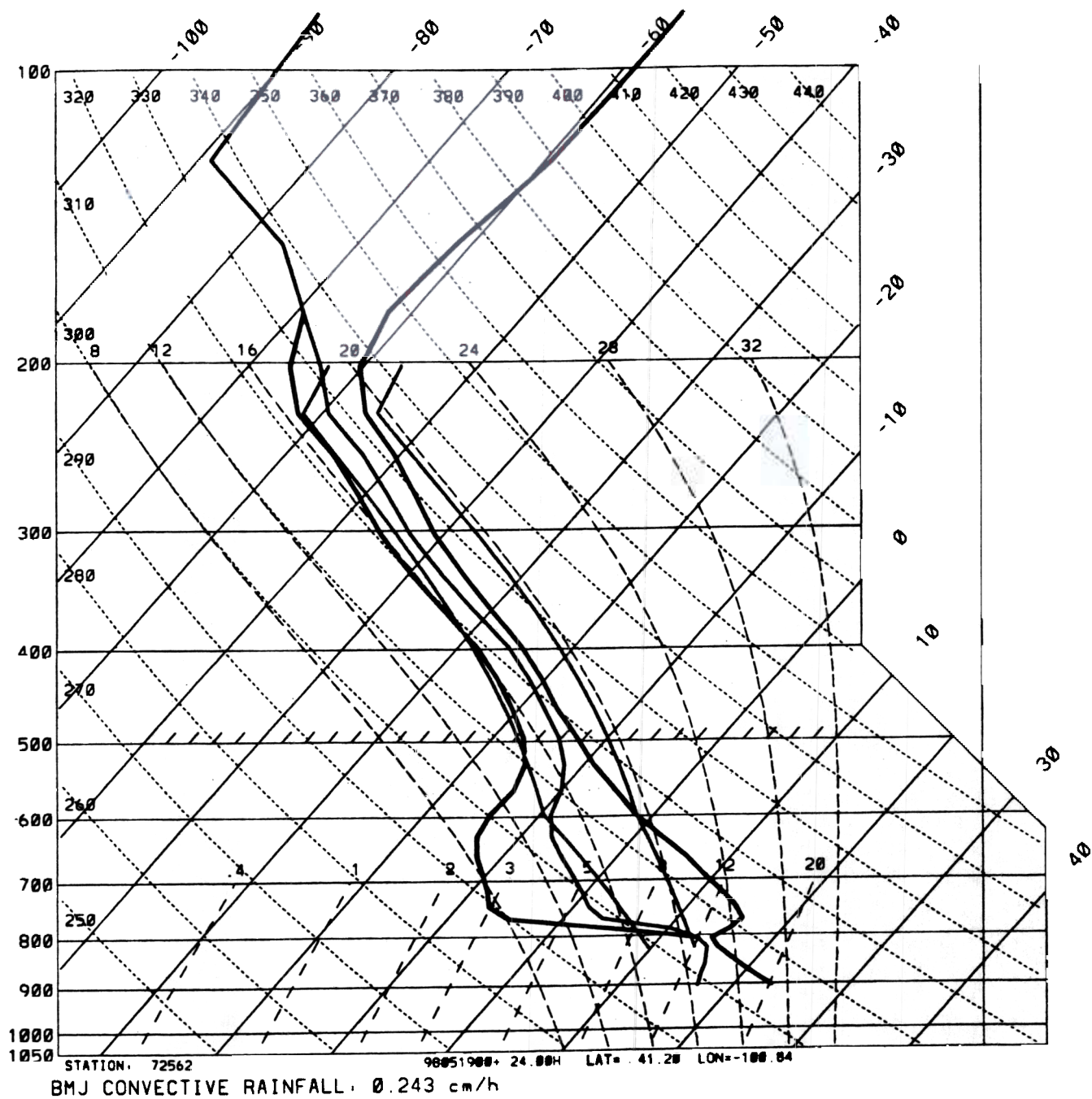


BMT HEATING (K/h)



# INCREASE CLOUD-LAYER R.H. BY 20%



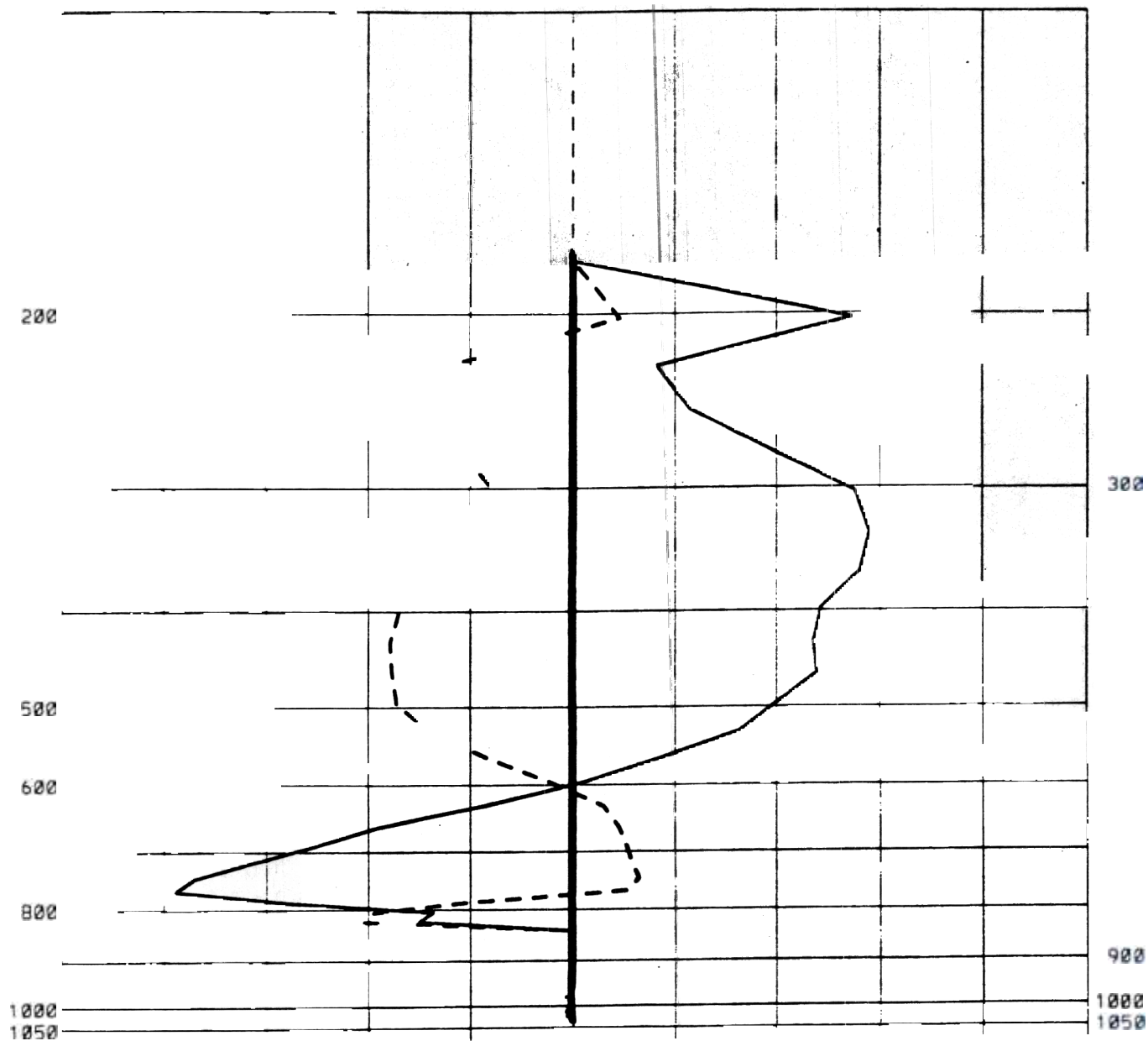


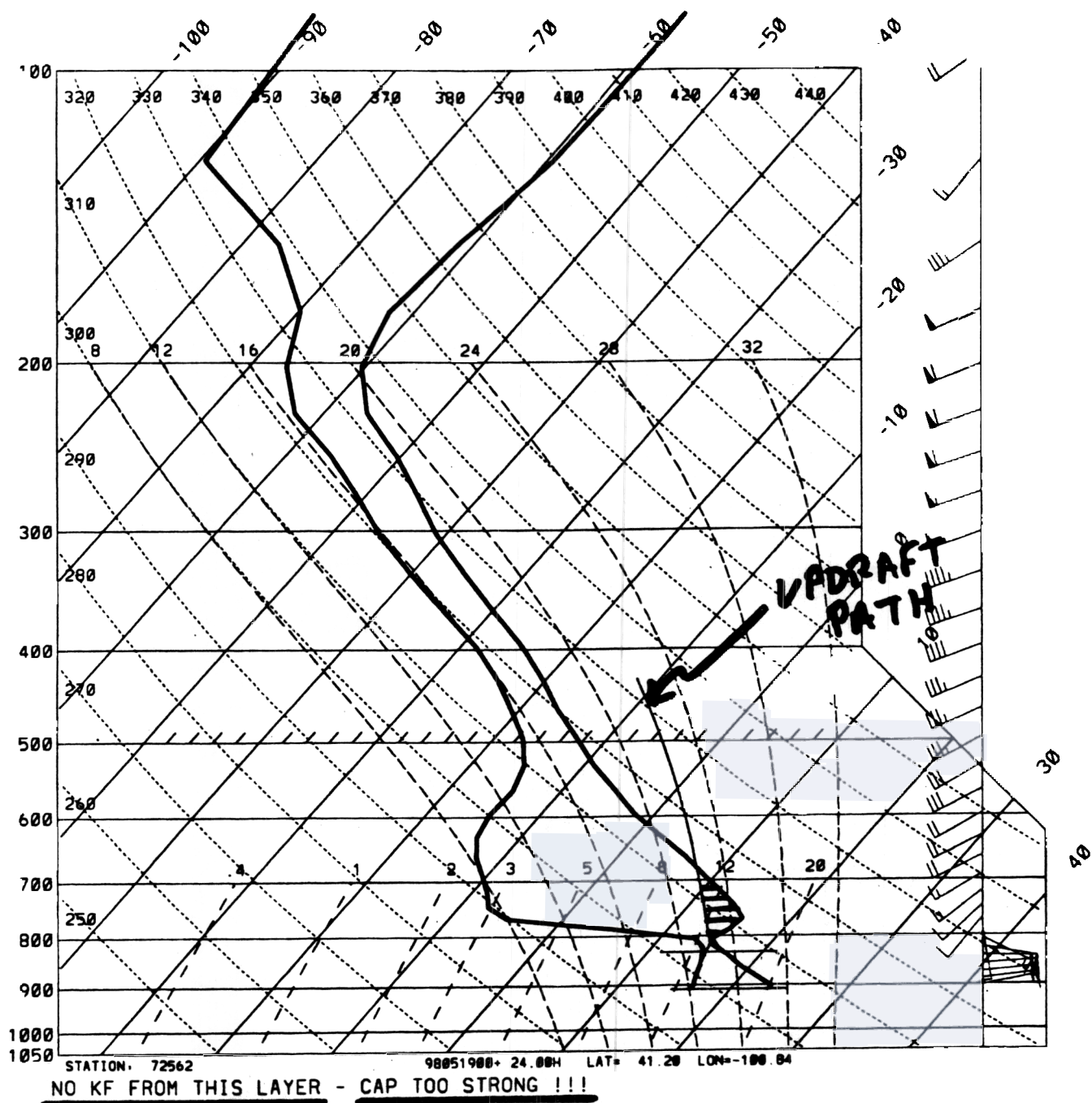
**DEEP CONVECTION ALLOWED**

ATION

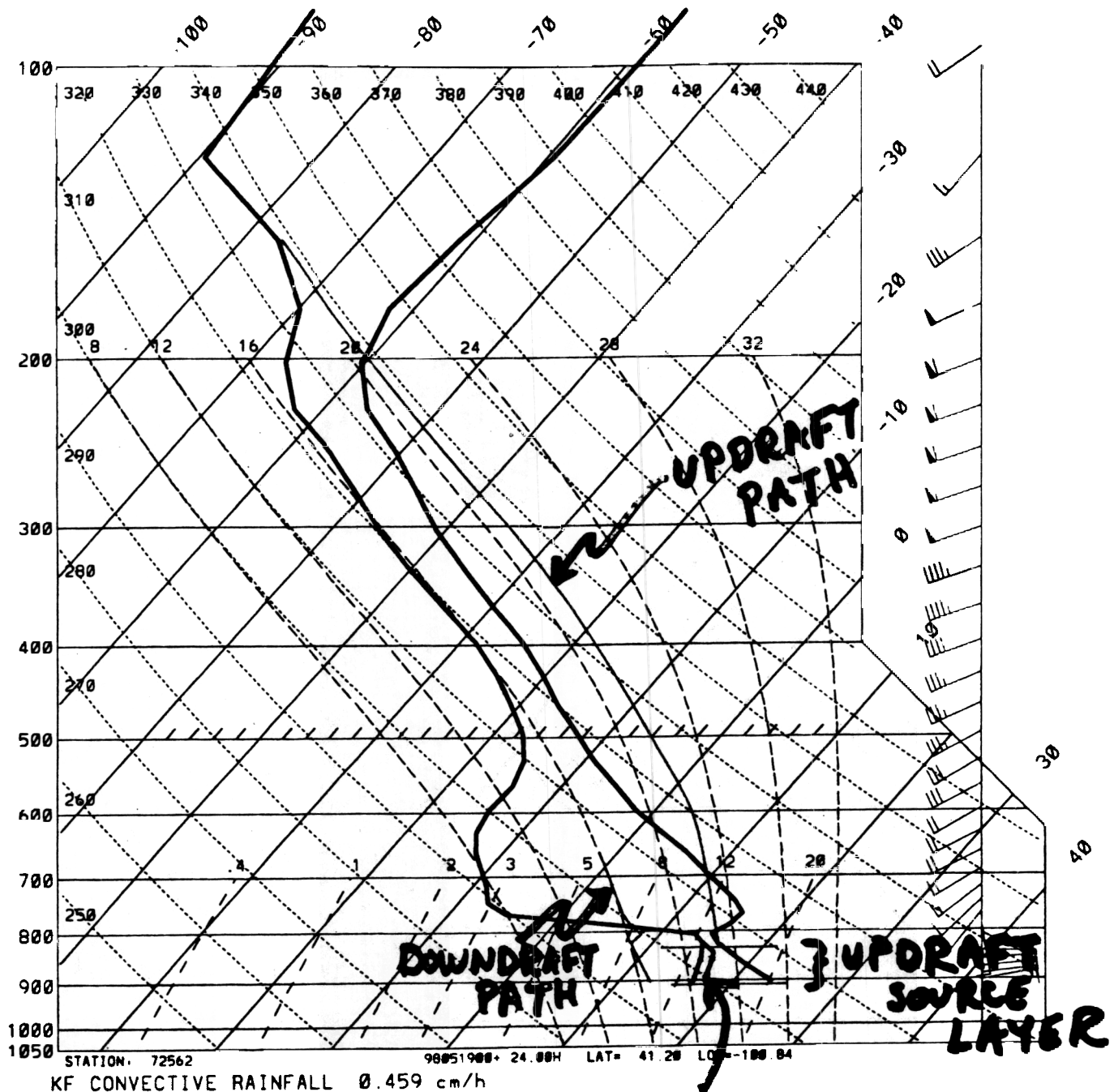
98051902

ON=-102





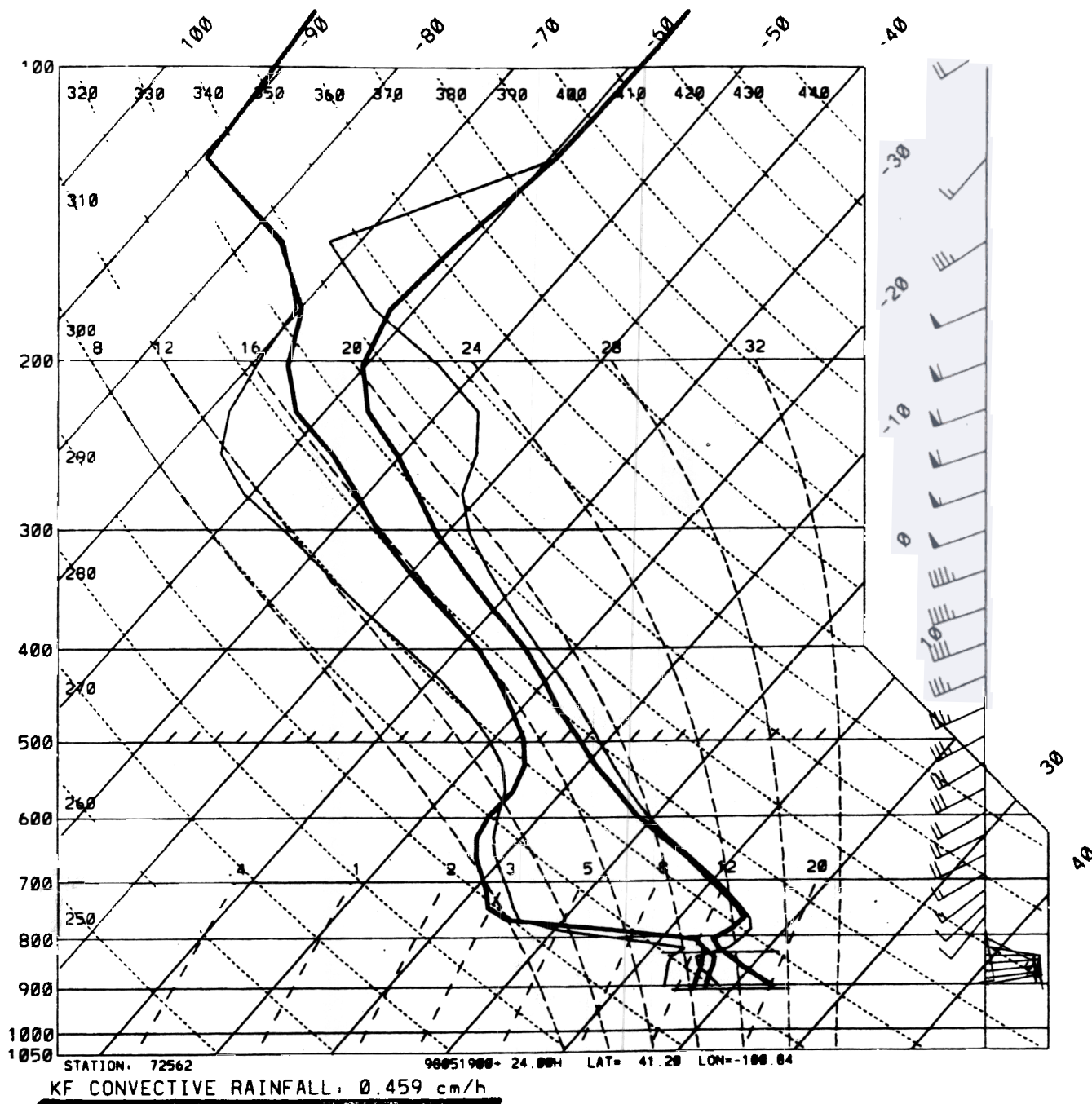
**KF TRIGGER: NO CONVECTION,  
CAP TOO STRONG!**



INCREASE SOURCE-  
 LAYER  $T_d$  BY  $1^\circ\text{C}$

KF TRIGGER: SOME PARCELS BREAK CAP,  
 INITIATE DEEP CONVECTION





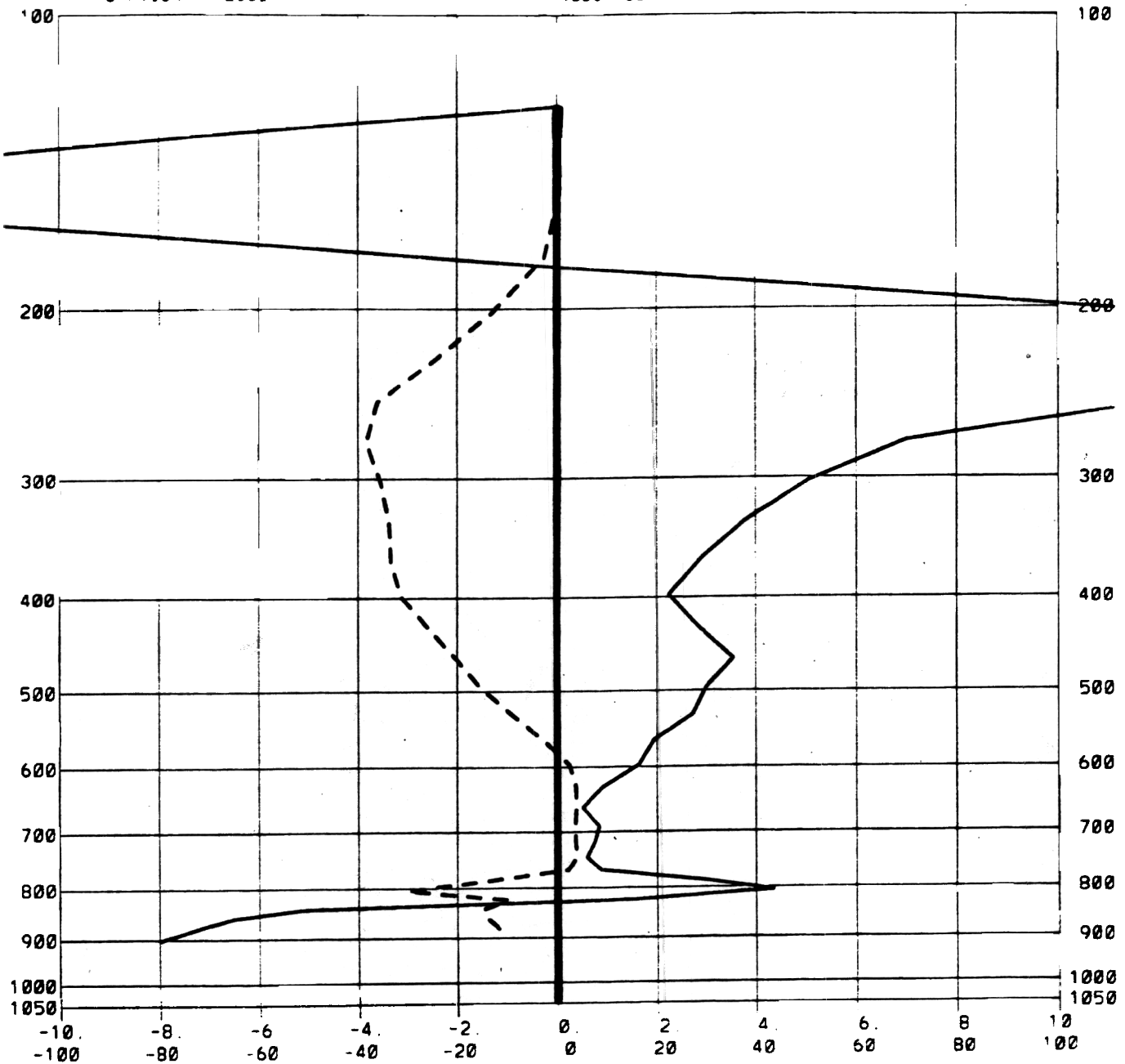
**KF CONVECTIVELY-ADJUSTED PROFILE**

STATION 72552

95051902- 24 00-

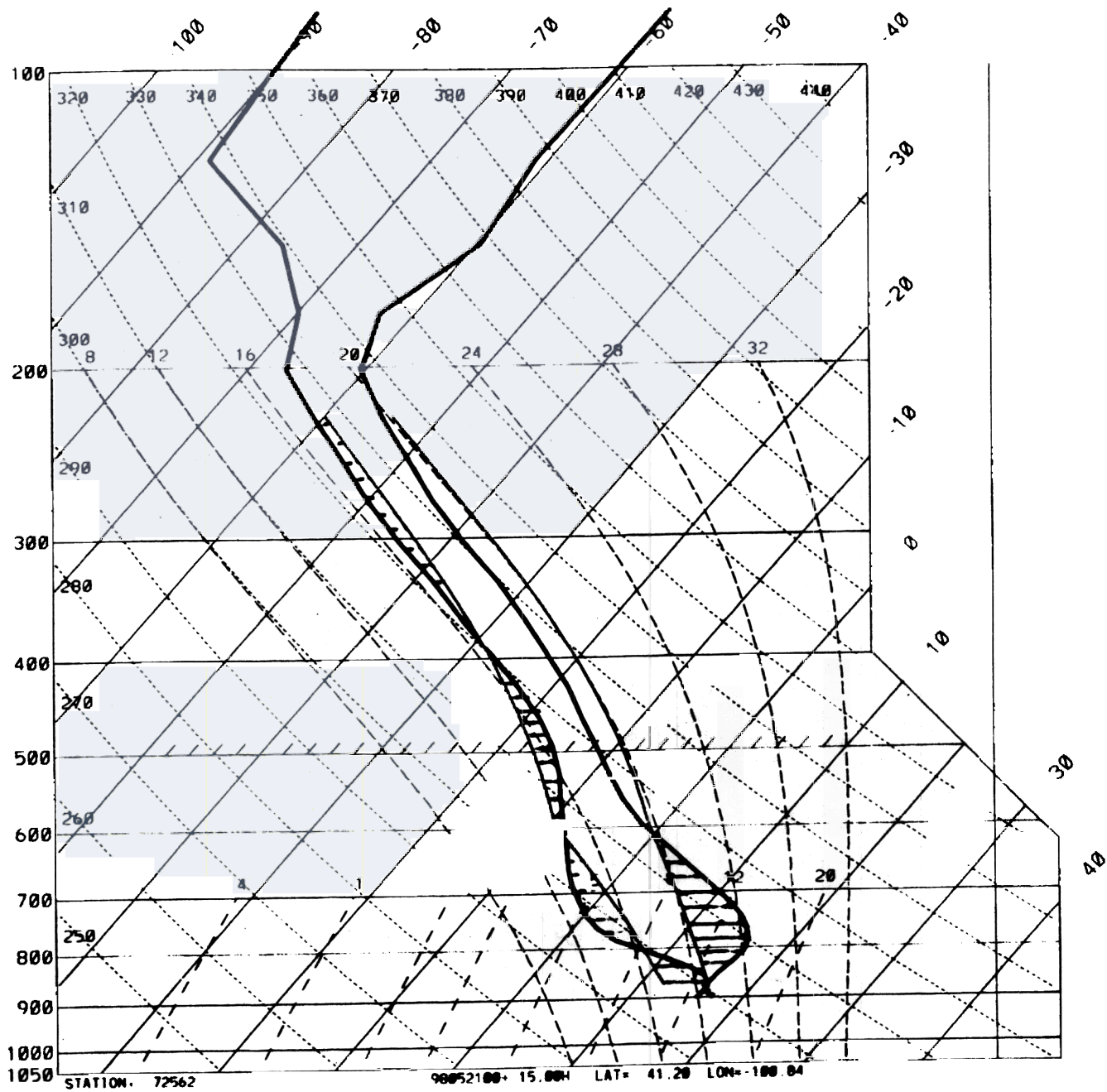
AT=

20 LON=-100 84

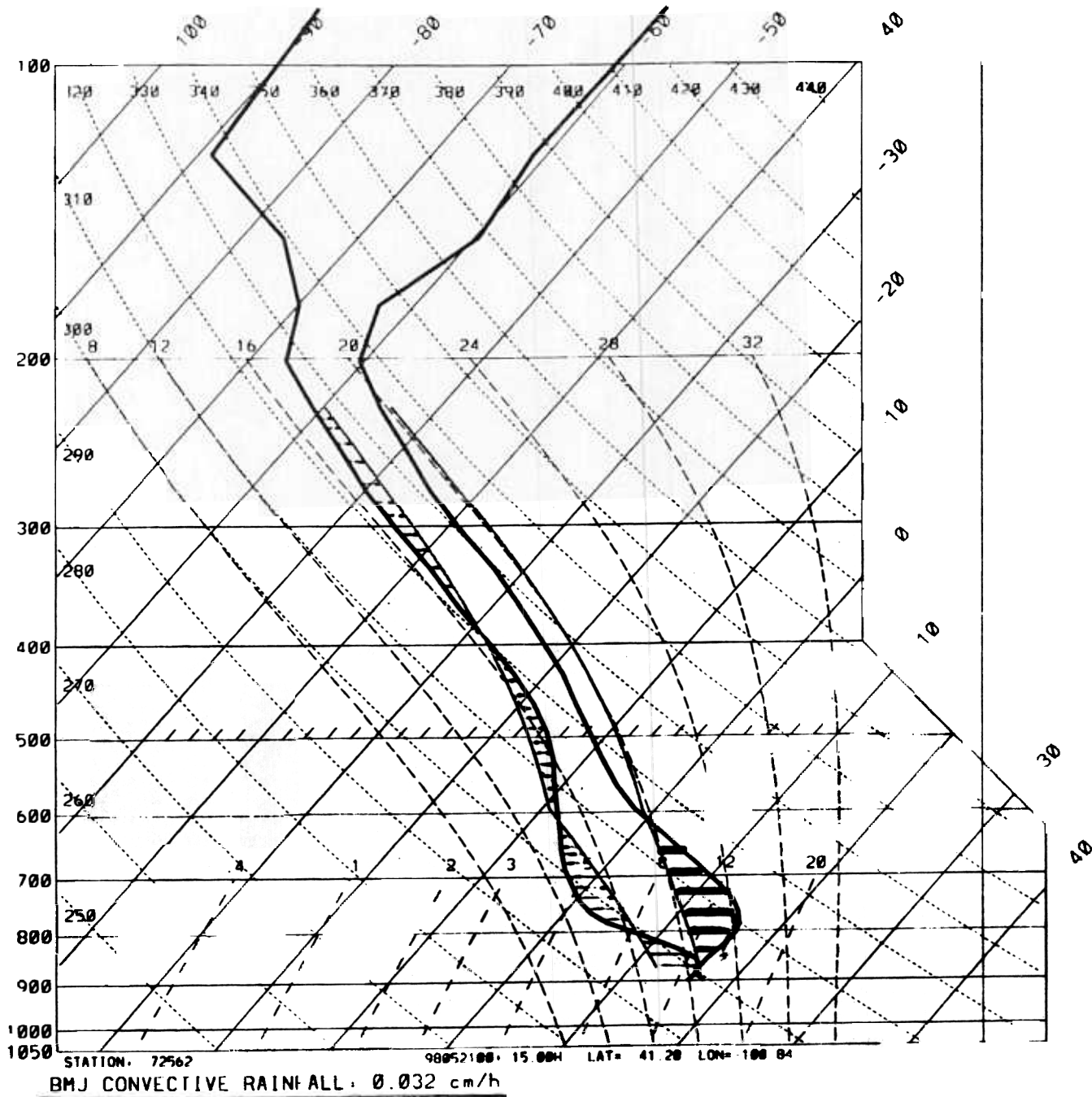


RF HEATING (K/h)

1 TAIL

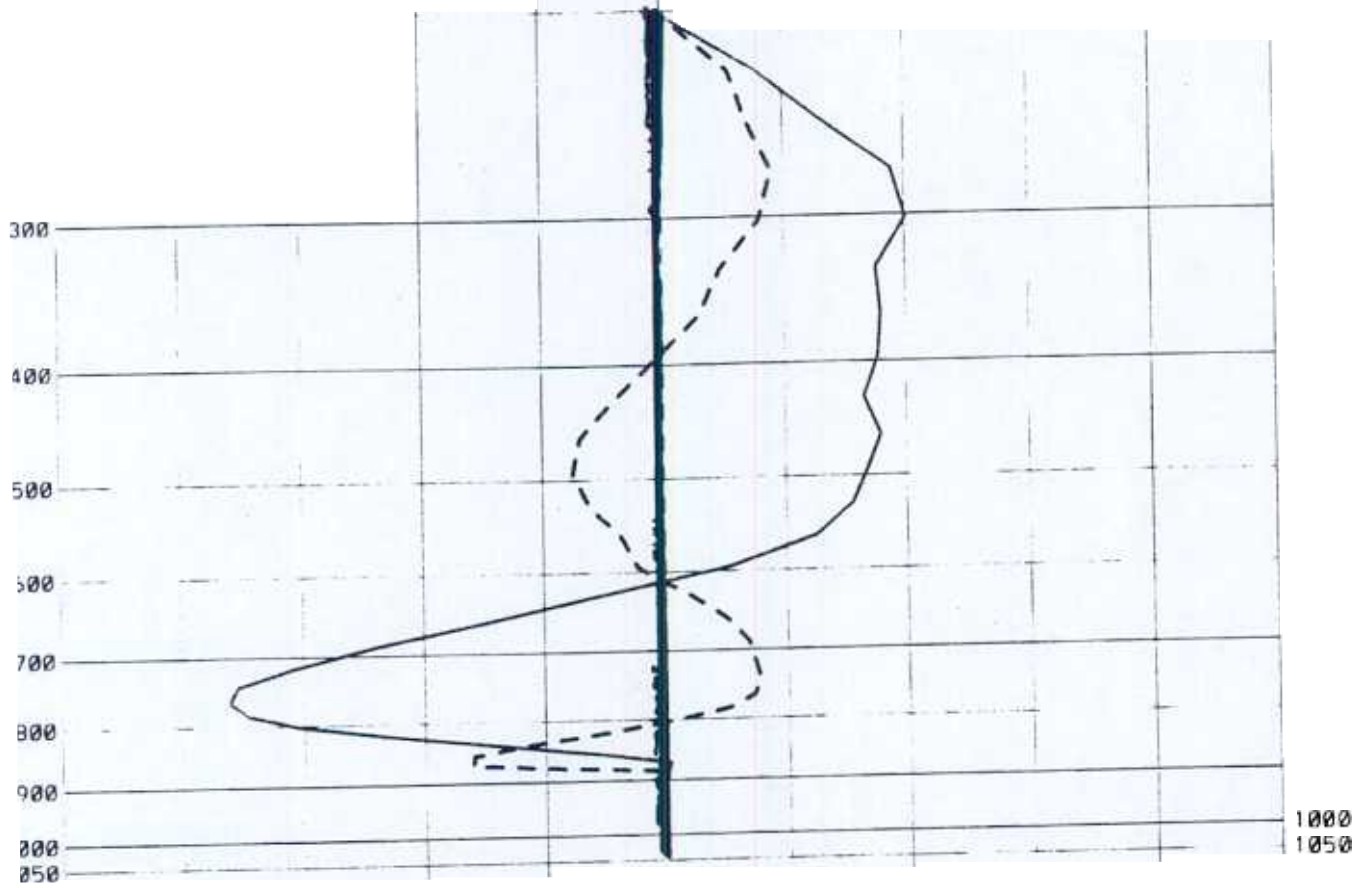


AFTER ENTHALPY ADJUSTMENT:  
DEEP CONVECTION ALLOWED



RAINFALL : 0.032 cm/h

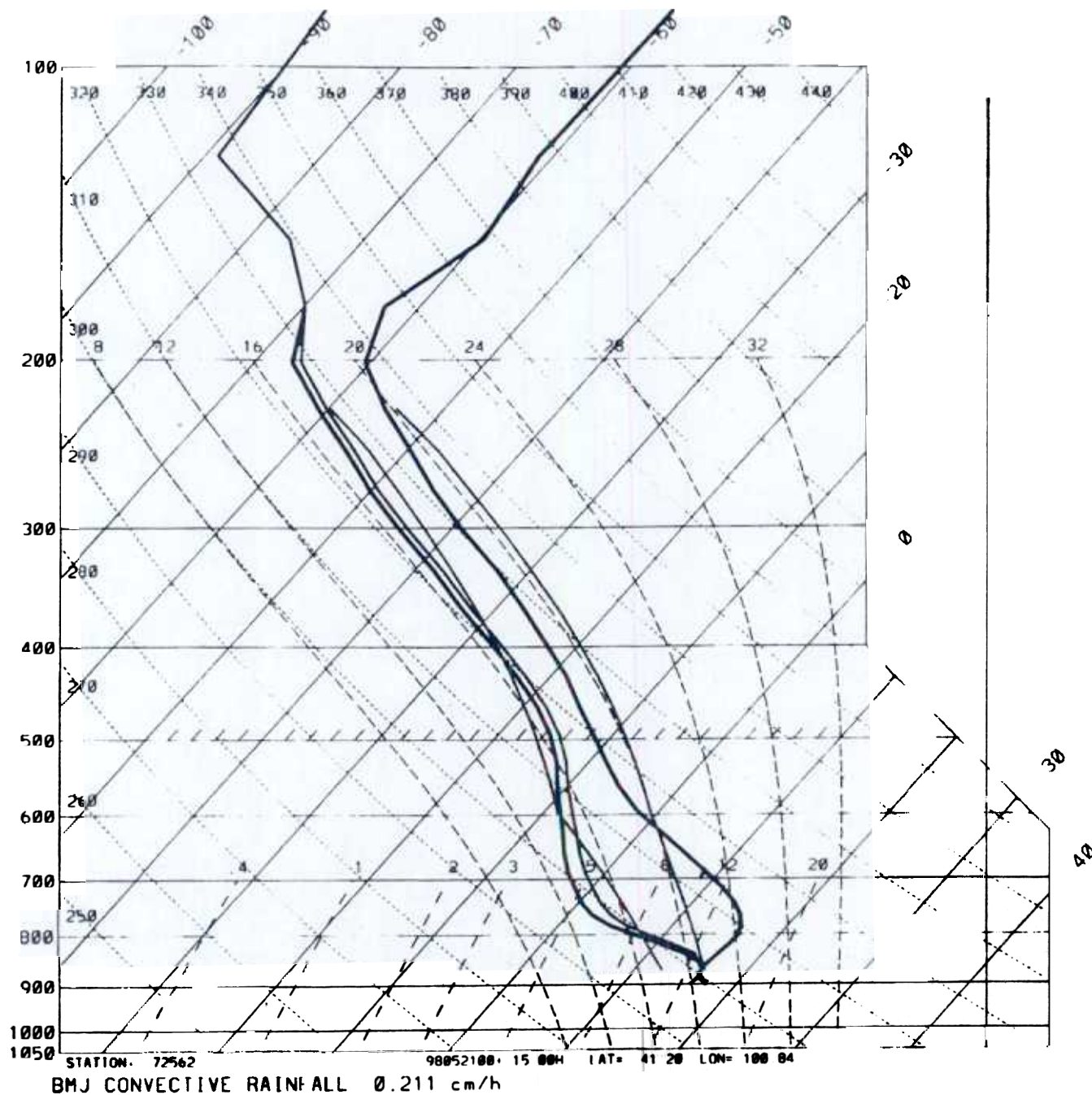
100



BMT HEATING (K/h)

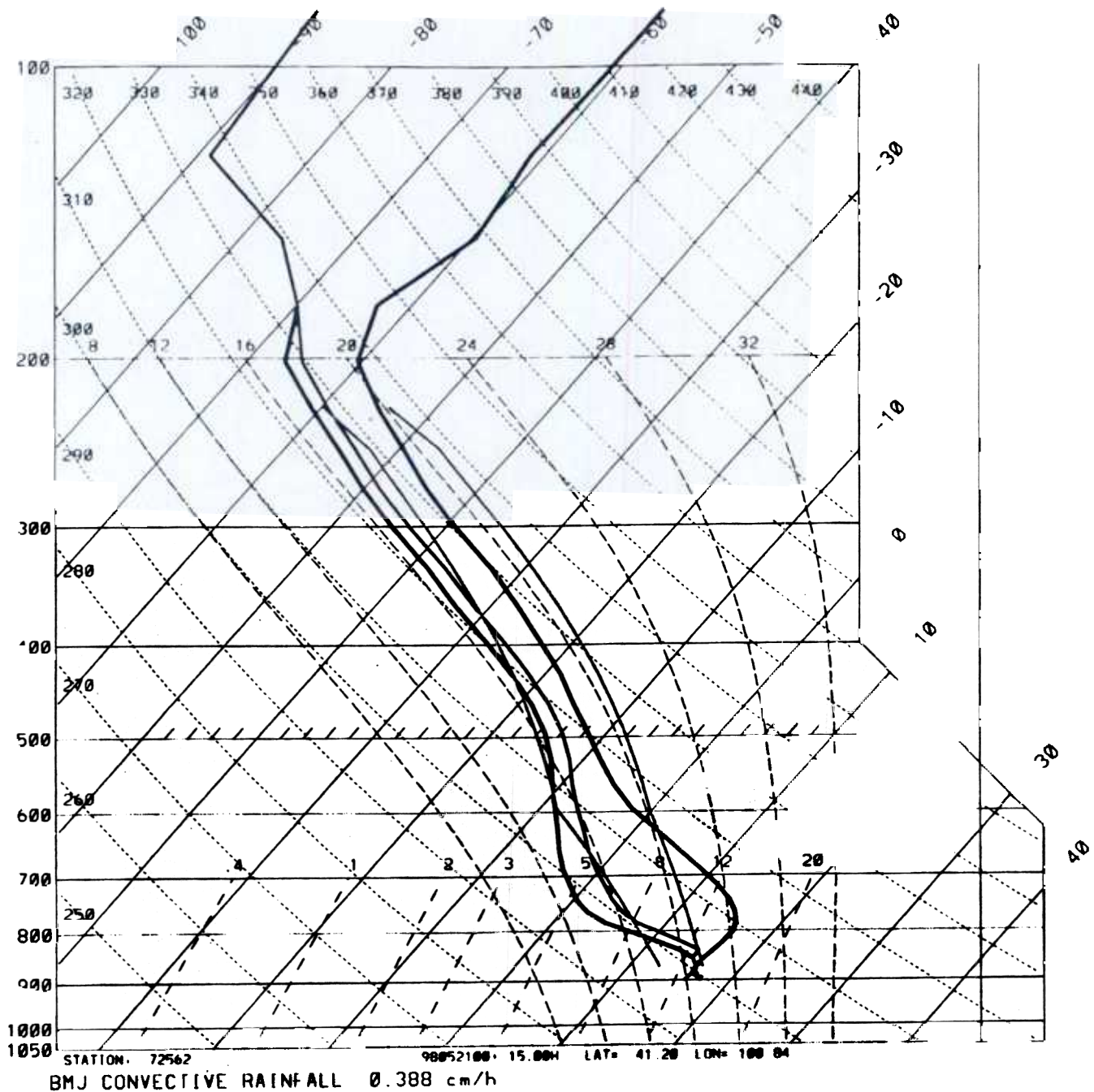


INCREASE CLOUD-LAYER R.H. BY 5%:



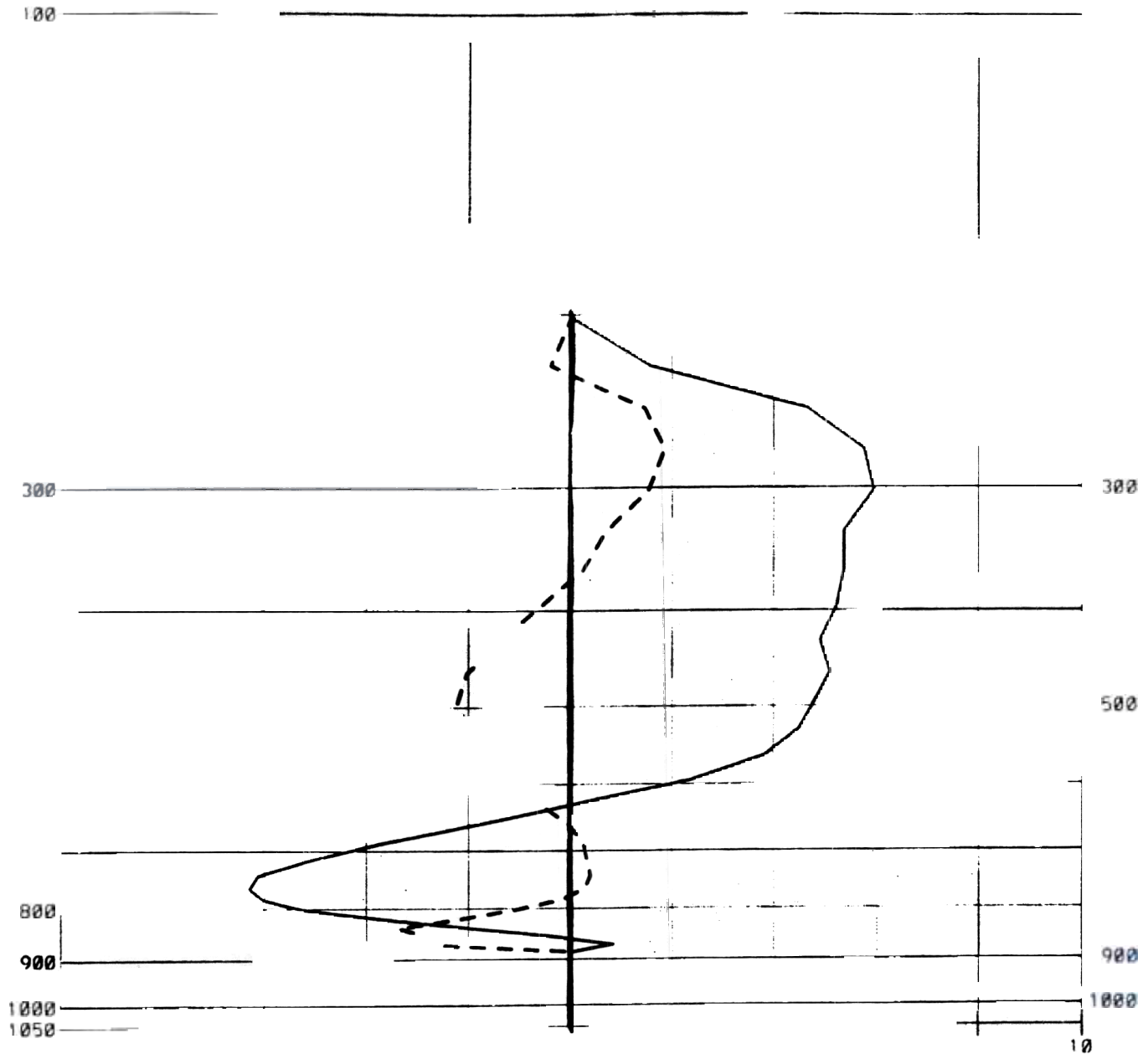
RAINFALL: 0.211 cm/h

INCREASE CLOUD-LAYER R.H. BY 10%



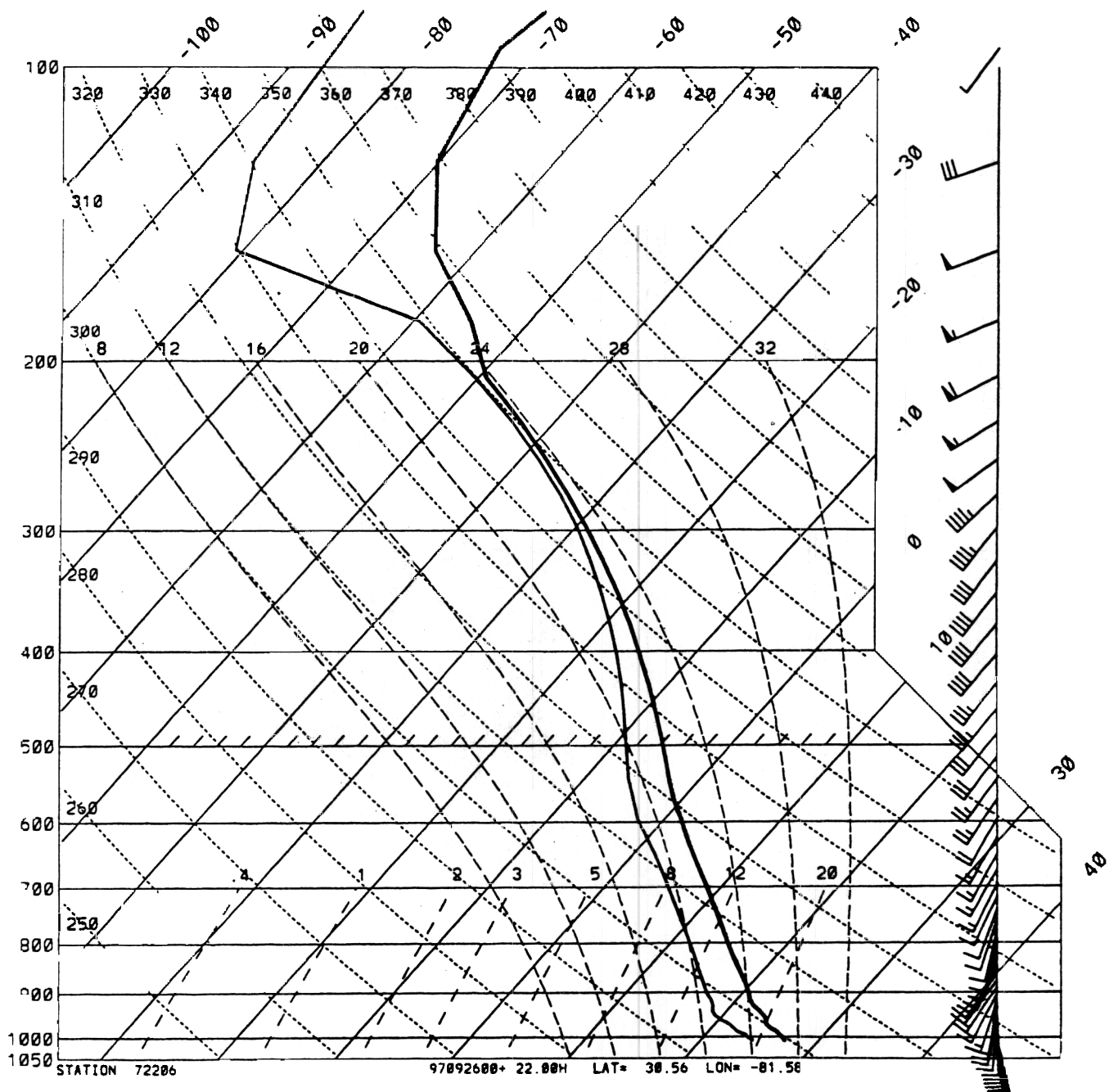
RAINFALL: 0.388 cm/h

$$d(RH) = 10\%$$



92

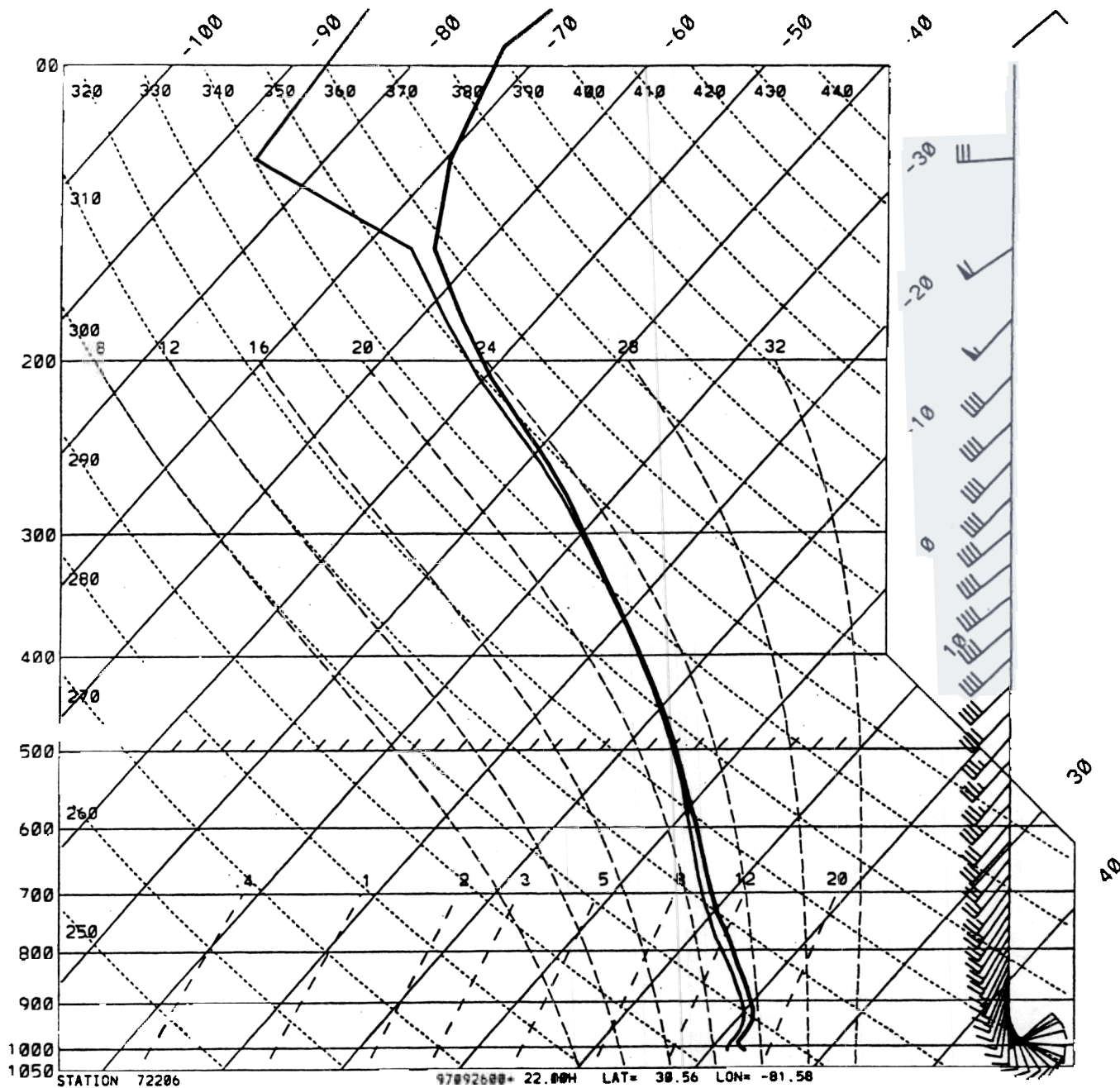
BMT HEATING (K/h)



Betts-Miller-Janjic Run  
 Predicted JAX Sounding  
 03Z 9/26/97 + 22 h

**HEAVY CONVECTIVE + NON CONVECTIVE RAIN**

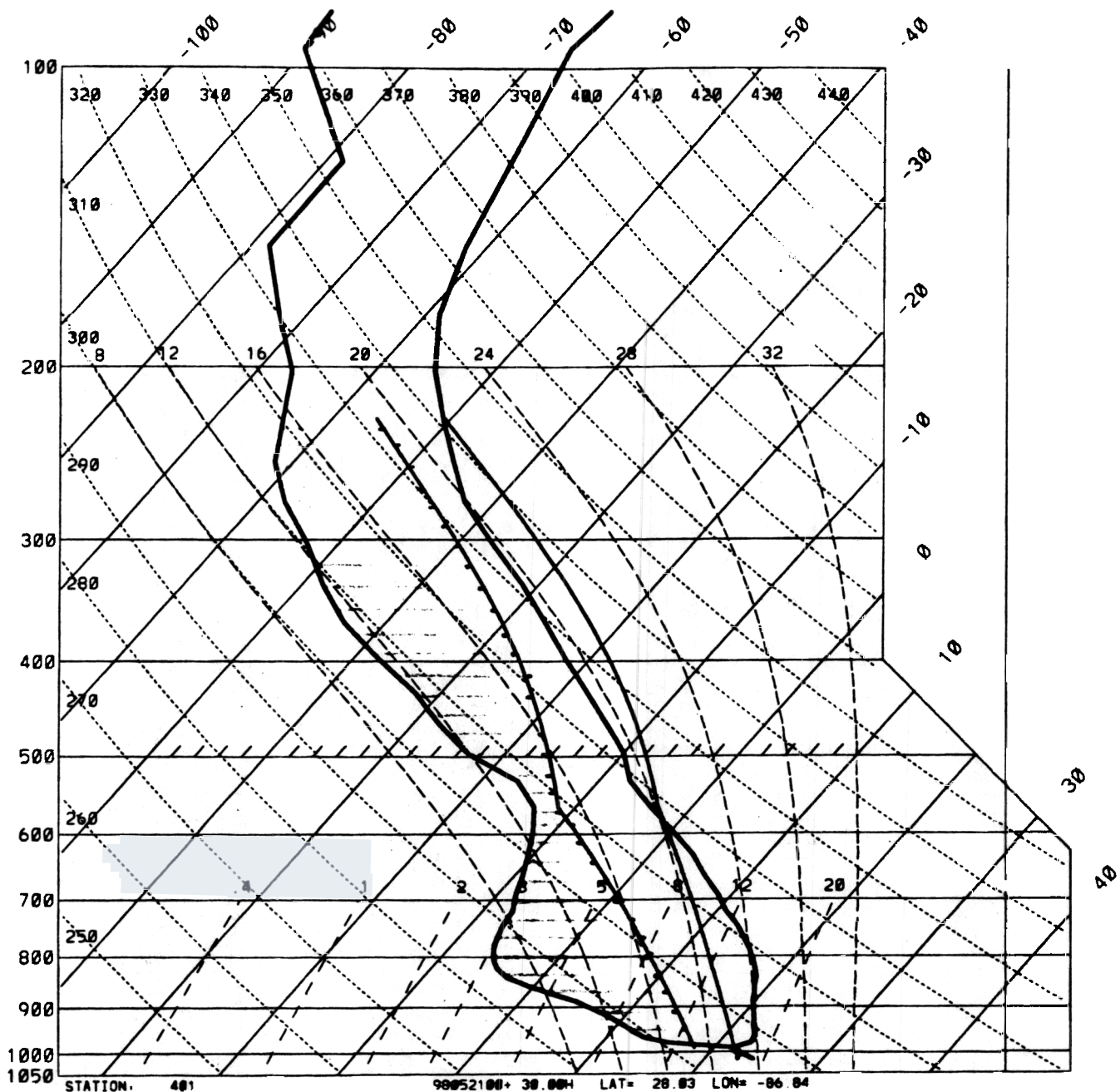




Kain-Fritsch Run  
 Predicted JAX Sounding  
 03Z 9/26/97 + 22 h

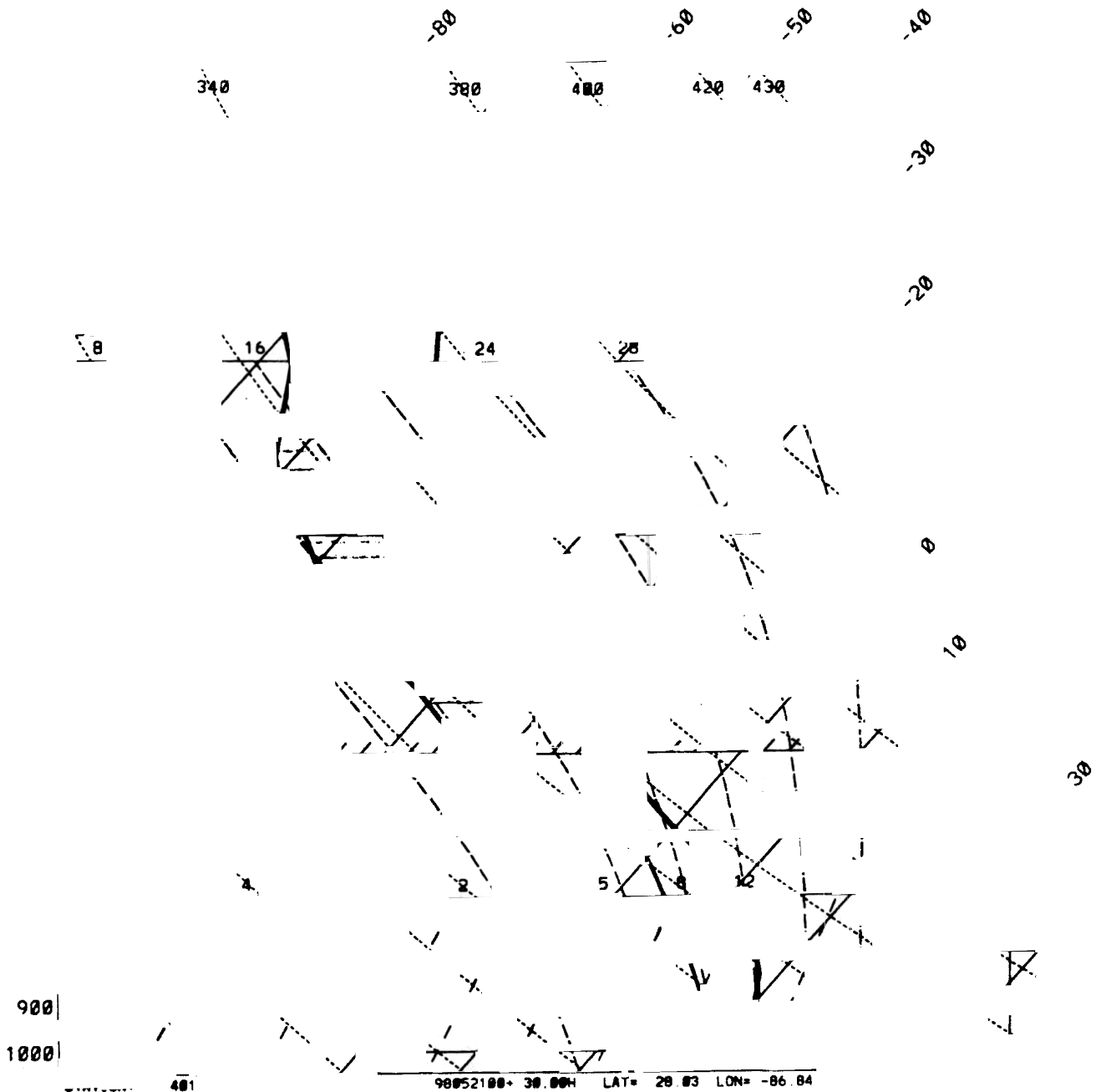
**HEAVY CONVECTIVE + NONCONVECTIVE RAIN**



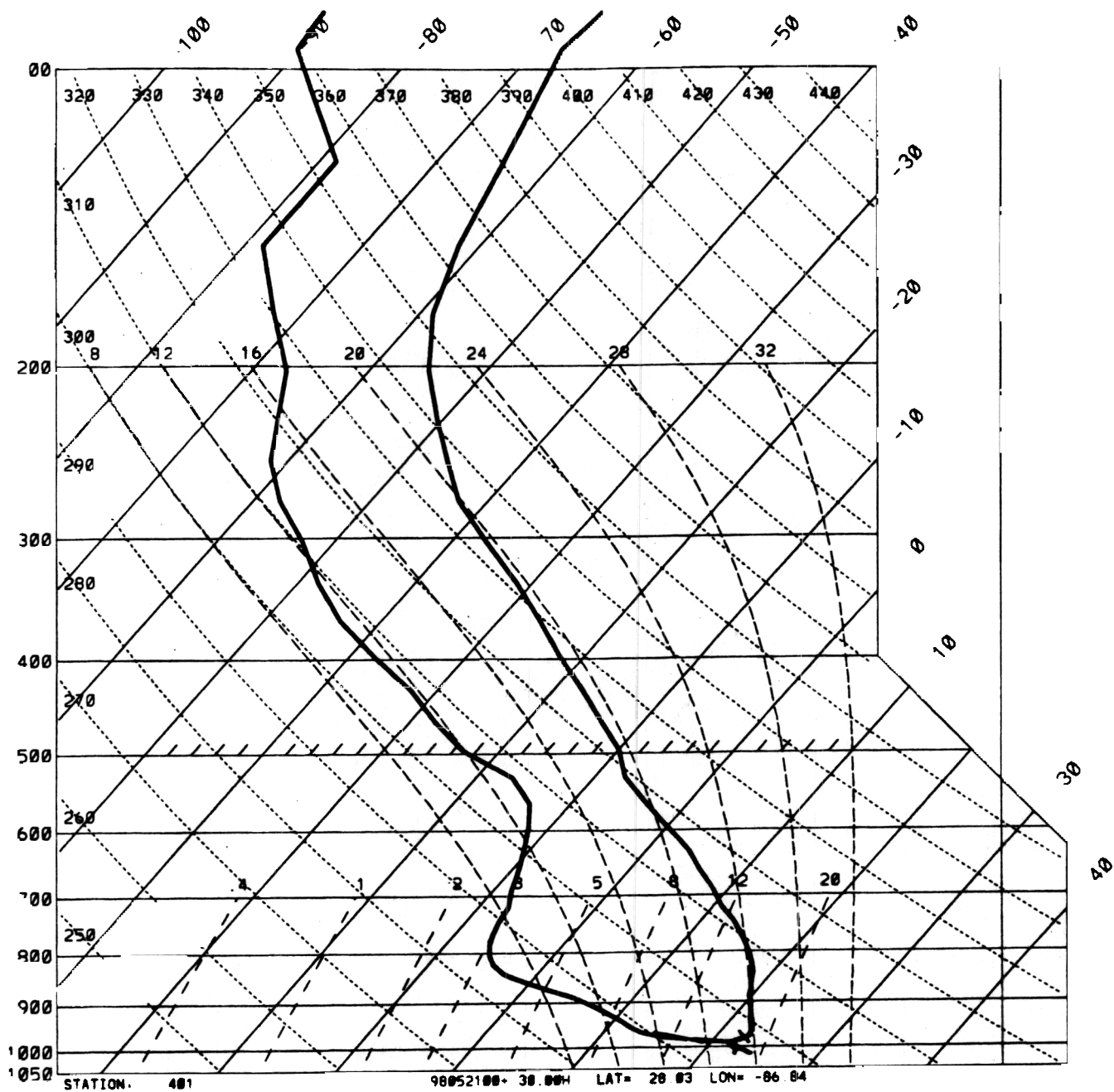


FIRST GUESS BMJ ADJUSTMENT PROFILE

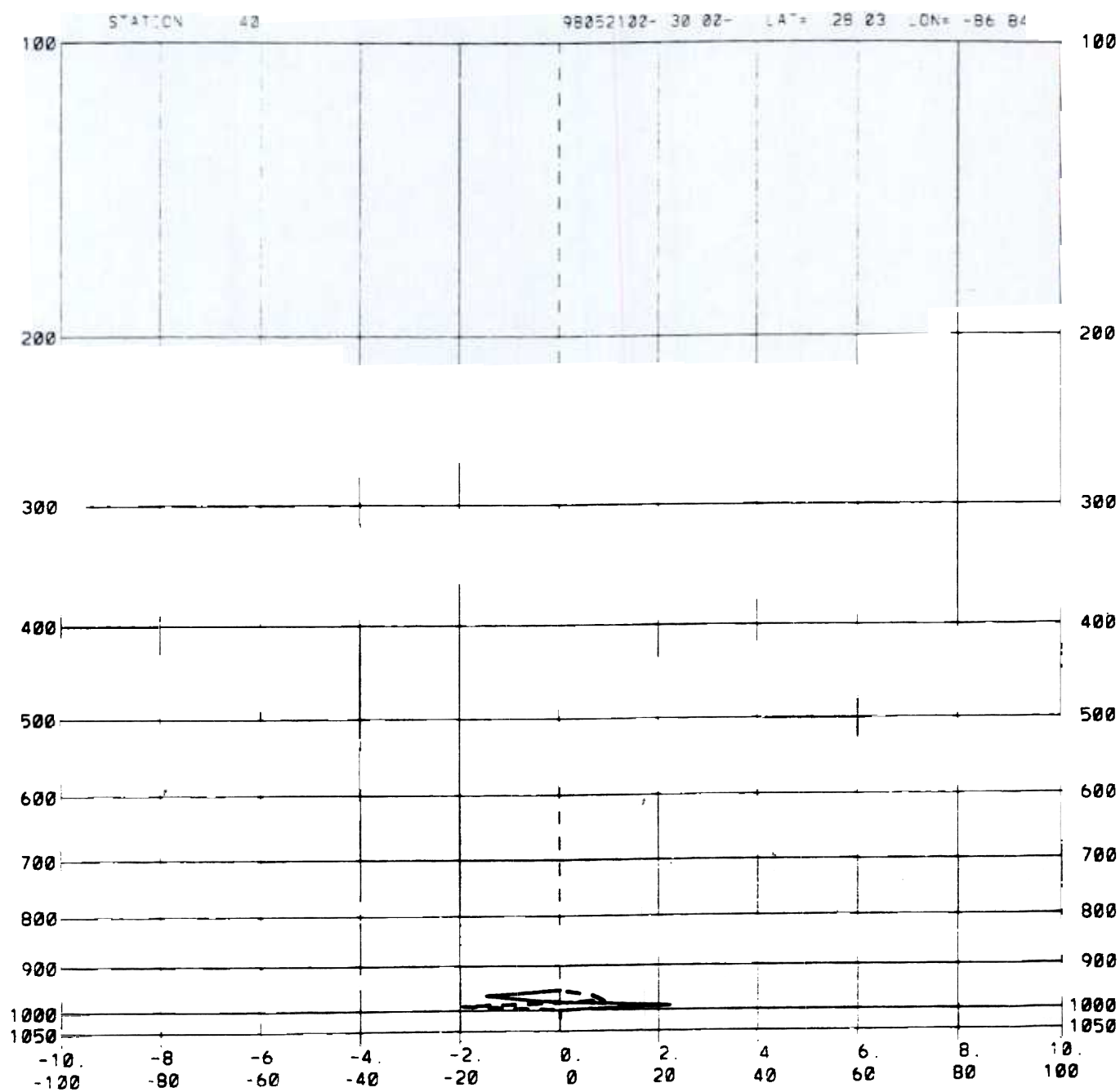
**OVER GULF OF MEXICO**

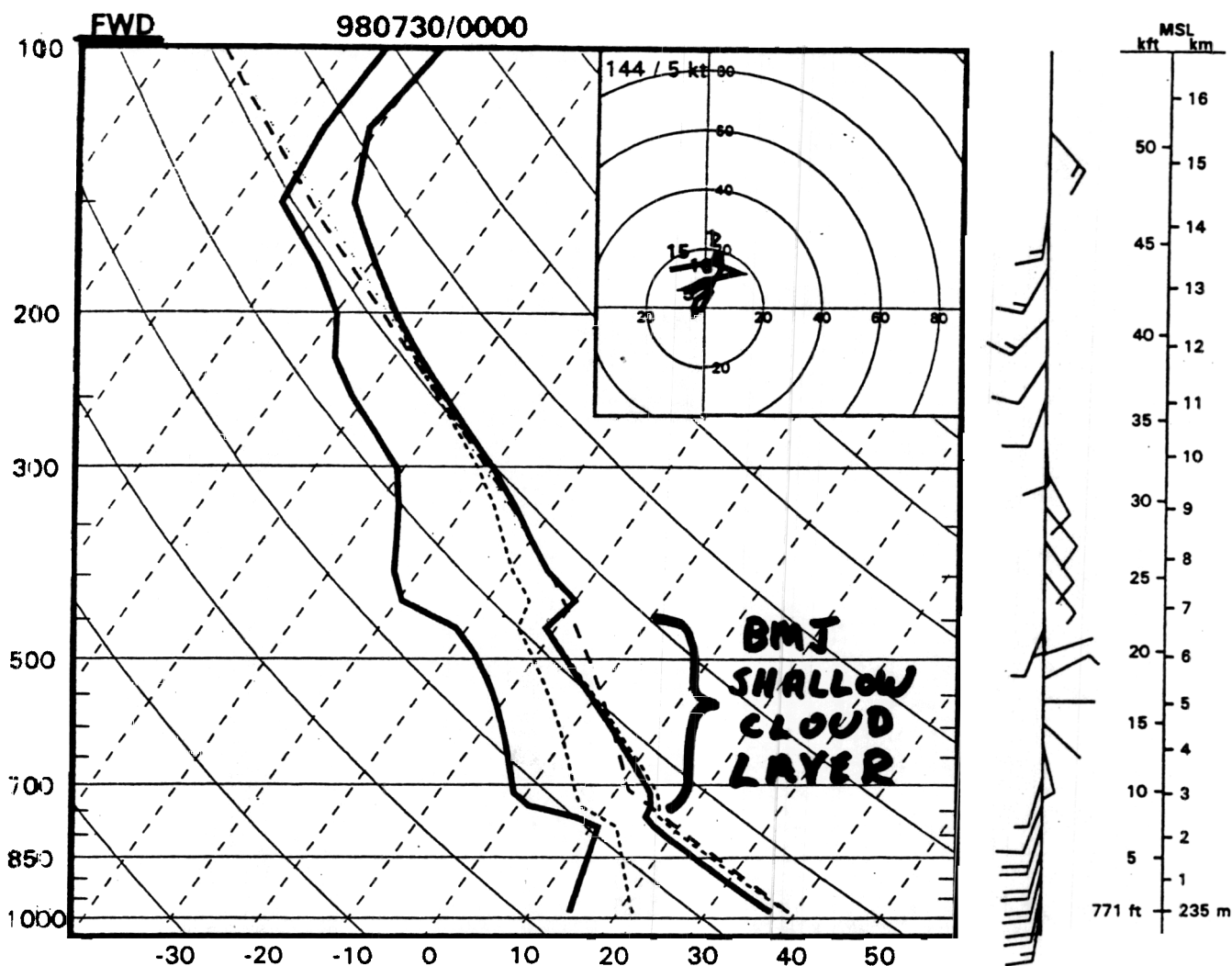


AFTER ENTHALPY CORRECTION - NEGATIVE PRECIP!!



BMJ SHALLOW CONVECTION; NO RAINFALL!!!!





### THERMODYNAMIC PARAMETERS

#### MOST UNSTABLE PARCEL

LPL: 984mb 37C/ 14C 99F/ 58F

CAPE: 136 J/kg LI: M

BFZL: 3 J/kg LImIn: 0 C @ 332mb

CINH: -87 J/kg CAP: 3 C @ 687mb

| LEVEL | PRES  | HGT(AGL) | TEMP  |
|-------|-------|----------|-------|
| LCL   | 709mb | 9392ft   |       |
| LFC   | 396mb | 24591ft  | -16 C |
| EL    | 358mb | 27013ft  | -21 C |
| MPL   | 363mb | 26680ft  |       |

Precip Water: 1.40 in Mean RH: 36 %  
 Mean Q: 10.6 g/kg Mean LRH: 35 %  
 Top of Moist Layer: 762 mb / 7372 ft

700-500mb Lapse Rate: 19 C / 7.2 C/km

850-500mb Lapse Rate: 32 C / 7.3 C/km

Total Totals: 49 K-Index: 28

SWEAT Index: 186 Max Temp: 102 F

ThetaE Diff: 49 Conv Temp: 102 F

FRZ Level: 15845 ft WBZ Level: 12901 ft

### KINEMATIC PARAMETERS

Sfc - 6 km Mean Wind: 118 / 3 kt (1 m/s)

LFC - EL Mean Wind: 144 / 7 kt (3 m/s)

850 - 300 Mean Wind: 185 / 8 kt (4 m/s)

Sfc - 2 km Shear: 2 kt (1 m/s) 4.37

Sfc - 6 km Shear: 17 kt (9 m/s) 42.64

\*BRN Shear: 4 m2/s2

### STORM STRUCTURE PARAMETERS

Sfc-3 km SREH: 22 m2/s2

Effective SREH: 22 m2/s2 from 0 m.

0-2 km SRW: 15 m/s EHI: 0

4-6 km SRW: 4 m/s BRN: 31

6-10 km SRW: 2 m/s