

Thermal Wind

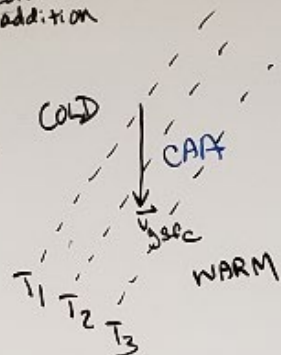
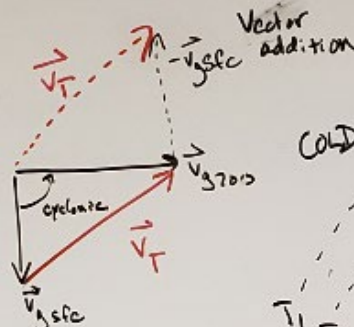
Orientation of thermal wind vector is parallel to thickness lines, of isotherms

Colder values are to LEFT of \vec{V}_T in NH

$$\vec{v}_{g700} - \vec{v}_{gsfc} = \vec{v}_T$$

Behind a cold front
CAA

Backing winds
Rotate cyclonically

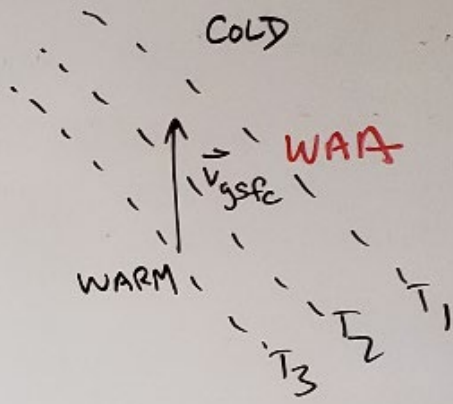
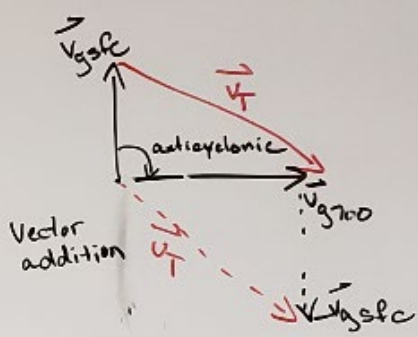


Northerly @ sfc
westerly aloft

$$T_3 > T_2 > T_1$$

Vicinity of warm front
WAA

Veering winds
Rotate anticyclonically



Southerly @ sfc
westerly aloft

Vorticity

In layman's terms a measure of spin in the atmosphere. Maximum in vorticity often referred to (inarticulately) as a "piece of energy" by TV meteorologists.

Mathematically, curl of the wind

$$\nabla \times \vec{v} = \vec{\zeta} \quad \vec{v} = (u, v, w)$$

A vector quantity

$$\nabla \times \vec{v} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ u & v & w \end{vmatrix} \begin{matrix} \hat{i} & \hat{j} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ u & v \end{matrix}$$

$$= \left(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) \hat{i} + \left(\frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right) \hat{j}$$

$$+ \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \hat{k}$$

Three components!

In synoptic meteorology because we assume $w \ll u, v$, we are typically concerned with just the vertical (\hat{k}) component of vorticity.

$$\hat{k} \cdot (\nabla \times \vec{v}) = \zeta_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \rightarrow \text{Relative (local) vorticity}$$

Can estimate on a Wx map (upper air chart) by a finite difference approach.

Vorticity equation (tendency)

$$\frac{\partial \zeta_z}{\partial t} = \underbrace{-\vec{v} \cdot \nabla \zeta_z}_{\text{B}} - \underbrace{\omega \frac{\partial \zeta_z}{\partial p}}_C - \underbrace{\left[\frac{\partial w}{\partial x} \frac{\partial v}{\partial p} - \frac{\partial w}{\partial y} \frac{\partial u}{\partial p} \right]}_D$$

A

$$+ \underbrace{\zeta_z \frac{\partial \omega}{\partial p}}_E + \underbrace{\left[\frac{\partial F_y}{\partial x} - \frac{\partial F_x}{\partial y} \right]}_F$$

* = Relevant for synoptic scale

Other terms ONLY important for mesoscale.

A = local time rate of change term

B = Horizontal vorticity advection
(PVA or NVA)

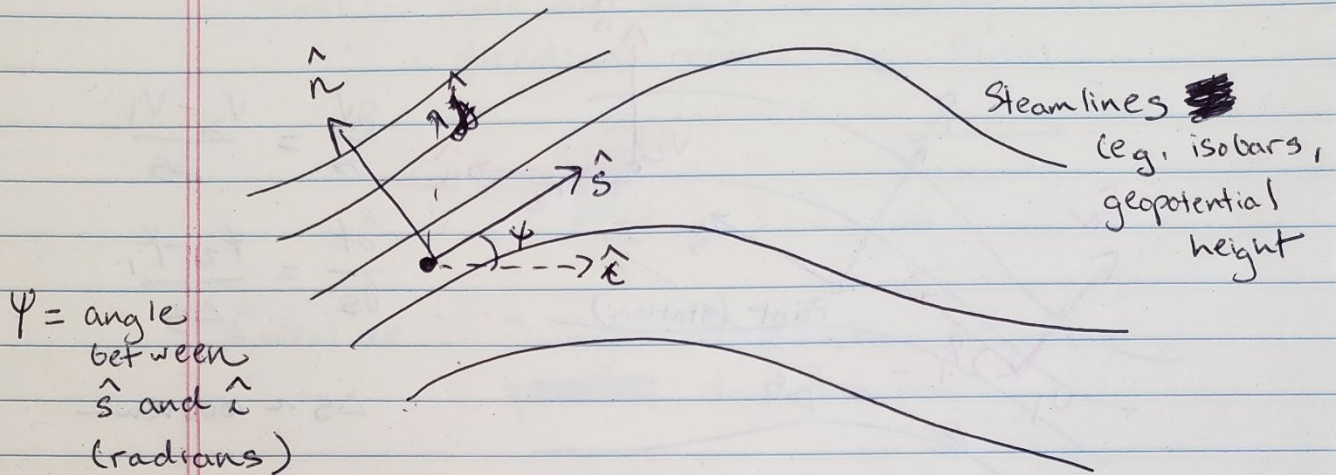
C = Vertical vorticity advection

D = Tilting of horizontal vorticity to
vertical

E = Vortex stretching (due to terrain,
diabatic heating)

F = Friction

Natural coordinate system



\hat{n} = vector normal to streamlines

\hat{s} = vector parallel to streamlines

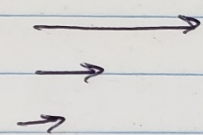
Vorticity and divergence

Vorticity $\hat{k} \cdot \nabla \times \vec{V}$ $|\vec{V}| \frac{\partial \psi}{\partial s} - \frac{\partial |\vec{V}|}{\partial n}$ $f_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y}$

Divergence $\nabla \cdot \vec{V}$ $|\vec{V}| \frac{\partial \psi}{\partial n} + \frac{\partial |\vec{V}|}{\partial s}$ $\text{DIV} = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}$

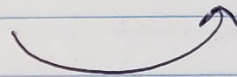
Other important kinematic flow properties

Shear : Rate of change of velocity in direction normal to flow

$$-\frac{\partial |\vec{V}|}{\partial n}$$


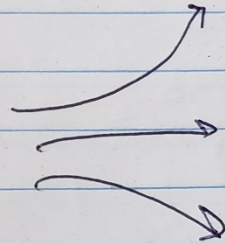
Curvature : Change in direction of flow ~~per~~ downstream

$$|\vec{V}| \frac{\partial \psi}{\partial s}$$



Diffluence : ^{Rate of} Change of the direction of flow normal to motion

$$|\vec{V}| \frac{\partial \psi}{\partial n}$$



Stretching : Rate of change of flow in downstream direction

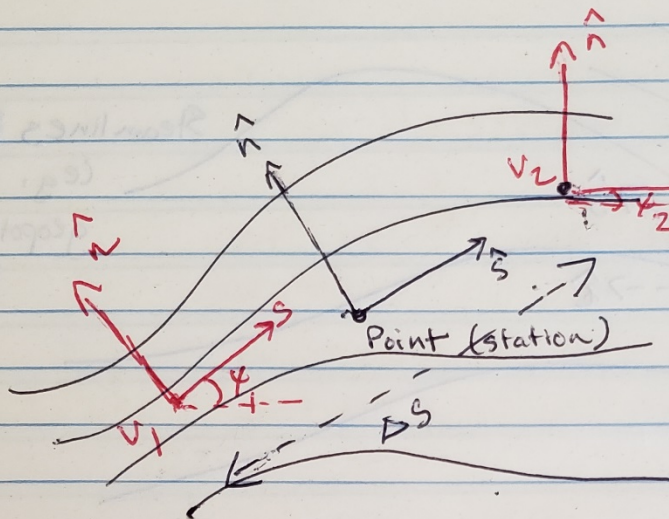
$$\frac{\partial |\vec{V}|}{\partial s}$$



Vorticity = Curvature + Shear

Divergence = Diffluence + Stretching

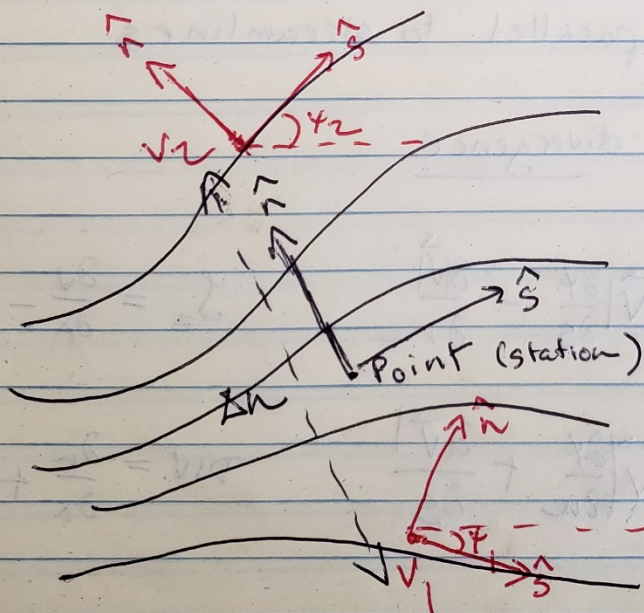
Suggested procedure for calculations of ψ derivative terms in natural coordinates!



$$\frac{\partial V}{\partial s} = \frac{V_2 - V_1}{\Delta s}$$

$$\frac{\partial \psi}{\partial s} = \frac{\psi_2 - \psi_1}{\Delta s}$$

$$\Delta s \sim 1000 \text{ km}$$



$$\frac{\partial V}{\partial n} = \frac{V_2 - V_1}{\Delta n}$$

$$\frac{\partial \psi}{\partial n} = \frac{\psi_2 - \psi_1}{\Delta n}$$

$$\Delta n \sim 1000 \text{ km}$$

ψ angle in radians

Quasi-geostrophic theory

Basic idea: What is a way we can account for the effect of advection by the geostrophic wind on vertical motion?

QG will provide us an equation that we can derive vertical motion based on synoptic-scale criteria. These are:

- Vorticity advection (PVA, NVA)
- Temperature advection (WTA, CAA)
- Diabatic heating (\dot{Q})

Again, where QG applies corresponds well with our definition of synoptic-scale we've been developing so far.

- Small Rossby number ($R_0 < 0.1$)
- Ageostrophic wind about 10% of v_g
- Adiabatic, frictionless
- Uniform static stability
- Hydrostatic balance.

Derivation of QG Vorticity Equation

Start with full equation of motion:

$$\frac{\partial u}{\partial t} = -u \frac{\partial u}{\partial x} - v \frac{\partial u}{\partial y} - \omega \frac{\partial u}{\partial p} - \frac{\partial \Phi}{\partial x} + f v$$

$$\frac{\partial v}{\partial t} = -u \frac{\partial v}{\partial x} - v \frac{\partial v}{\partial y} - \omega \frac{\partial v}{\partial p} - \frac{\partial \Phi}{\partial y} - f u$$

Quasi-geostrophic system:

$$\frac{d}{dt} = \frac{\partial}{\partial t} + \vec{v}_g \cdot \nabla_h = \frac{\partial}{\partial t} + u_g \frac{\partial}{\partial x} + v_g \frac{\partial}{\partial y}$$

Consider variation of f with latitude

$$f = f_0 + \frac{\partial f}{\partial y} y \quad \underline{\text{or}} \quad f_0 + \beta y$$

$$\frac{d\vec{v}_g}{dt} = -\nabla \Phi - (f_0 + \beta y) \hat{k} \times \vec{v}$$

↑
Total
derivative

↑
($\vec{v}_g + \vec{v}_{ag}$)
geostrophic
+
ageostrophic

Using definition of geostrophic wind

$$\vec{v}_g = \frac{1}{f_0} \hat{k} \times \nabla \Phi$$

$$f_0 \hat{k} \times \vec{v}_g = -\nabla \Phi$$

Substitute for $-\nabla \Phi$ in equation for $d\vec{v}_g/dt_g$

$$\frac{d\vec{v}_g}{dt_g} = f_0 (\hat{k} \times \vec{v}_g) - (f_0 + \beta y) \hat{k} \times (\vec{v}_g + \vec{v}_g)$$

Terms with $f_0 (\hat{k} \times \vec{v}_g)$ cancel

$$\frac{d\vec{v}_g}{dt_g} = -f_0 \hat{k} \times \vec{v}_g - \beta y \hat{k} \times \vec{v}_g - \beta y \hat{k} \times \vec{v}_g$$

↑
to zero
by scaling

$$\frac{d\vec{v}_g}{dt_g} = -f_0 \hat{k} \times \vec{v}_g - \beta y \hat{k} \times \vec{v}_g$$

Expanding into components

$$(u_{eq}) \quad \frac{\partial u_g}{\partial t} + u_g \frac{\partial u_g}{\partial x} + v_g \frac{\partial u_g}{\partial y} - f_0 v_g - \beta y v_g = 0$$

$$(v_{eq}) \quad \frac{\partial v_g}{\partial t} + u_g \frac{\partial v_g}{\partial x} + v_g \frac{\partial v_g}{\partial y} + f_0 u_g + \beta y u_g = 0$$

Construct QG vorticity (f_g) by:

$$\frac{\partial}{\partial x} (v_{eq}) - \frac{\partial}{\partial y} (u_{eq}) = \frac{\partial f_g}{\partial t}$$

Using continuity

$$\frac{\partial u_{eq}}{\partial x} + \frac{\partial v_{eq}}{\partial y} + \frac{\partial w}{\partial p} = 0 \quad \text{and} \quad \frac{\partial u_{eq}}{\partial x} + \frac{\partial v_{eq}}{\partial y} = 0$$

QG
vorticity
equation

$$\frac{\partial f_g}{\partial t} = -\vec{v}_g \cdot \nabla_g (f_g + f_0) + f_0 \left(\frac{\partial w}{\partial p} \right)$$

where... $f_g = \frac{\partial v_g}{\partial x} - \frac{\partial u_g}{\partial y} = \frac{1}{f_0} \nabla^2 \Phi$
Laplacian of
geopotential

Differences with full vorticity equation $\partial f / \partial t$

Retained: Horizontal advection, vortex stretching

Neglected: Vertical advection, tilting,
friction.

QG Thermodynamic Equation

Adiabatic form:

$$\frac{\partial T}{\partial t} = -\vec{v}_g \cdot \nabla T + \frac{\gamma P}{R} \omega = 0$$

↑
Advection

↑
Adiabatic correction factor
for T , because not conserved
with vertical motion.

$$\sigma = -\frac{RT}{P} \frac{d \ln \theta}{dp} \rightarrow \text{Static stability!}$$

Assumed to be only
a function of pressure.

Diabatic:

$$\frac{\partial T}{\partial t} = -\vec{v}_g \cdot \nabla T + \frac{\sigma}{R} \omega + \left(\frac{J}{c_p} \right) \text{Heating term } (\dot{Q})$$

\dot{Q} sources / sinks:

- Latent heat release → most important one for synoptic scale!
- Radiation
- Friction

Q6 Omega Equation (Adiabatic)

Using thermodynamic equation, replace T by vertical derivative of geopotential ($\frac{\partial \Phi}{\partial p}$) which is related to T by hypsometric equation.

Then divide by $-P/R$, differs only by factor g_0

$$\frac{\partial}{\partial t} \left(\frac{\partial \Phi}{\partial p} \right) + \vec{v}_g \cdot \nabla \left(\frac{\partial \Phi}{\partial p} \right) + \sigma \omega = 0$$

$\chi =$ geopotential height tendency $= \frac{\partial \Phi}{\partial t}$

$$\boxed{\frac{\partial \chi}{\partial p} = -\vec{v}_g \cdot \nabla \frac{\partial \Phi}{\partial p} - \sigma \omega} \quad \text{Q6 thermodyn equation.}$$

Recall --

$$\frac{\partial \zeta_g}{\partial t} = \frac{1}{f_0} \frac{\partial}{\partial t} (\nabla^2 \Phi) = \frac{1}{f_0} \nabla^2 \chi$$

Substitute for $\zeta_g = \frac{1}{f_0} \nabla^2 \Phi$ in vorticity eqn.

$$\boxed{\nabla^2 \chi = -f_0 \vec{v}_g \cdot \nabla \left(\frac{1}{f_0} \nabla^2 \Phi + f_0 \right) + f_0^2 \frac{\partial \omega}{\partial p}}$$

Q6
vorticity
eqn.

Steps to derive final QG omega equation from here:

- Take ∇^2 (Thermodyn. eqn) - $\frac{\partial}{\partial p}$ (Vort. eqn)

- Divide by G

Result: QG omega equation

$$\left[\nabla^2 + \frac{f_0^2}{\sigma} \frac{\partial}{\partial p^2} \right] \omega = \frac{f}{\sigma} \frac{\partial}{\partial p} \left\{ \vec{v}_g \cdot \nabla \left(\frac{1}{f_0} \nabla^2 \Phi + F \right) \right\} \\ (A) \qquad \qquad \qquad (B) \\ + \frac{1}{\sigma} \nabla^2 \left\{ \vec{v}_g \cdot \nabla \left(-\frac{\partial \Phi}{\partial p} \right) \right\} \\ (C)$$

A diagnostic equation for ω that can be solved iteratively)

Physical interpretation

A: 3D Laplacian of ω

B: Vertical derivative of geostrophic vorticity advection by \vec{v}_g (differential vorticity advection)

Positive: PVA increasing with height
→ Ascent

Negative: NVA increasing with height
→ Descent

Likewise, converse if decreasing with height

Operational practice: Consider PVA, NVA at 500-mb (level of non-divergence)

C. Thermal advection

Warm Air Advection (WAA) \rightarrow Ascent

Cold Air Advection (CAA) \rightarrow Descent

Operational practice! Consider at 700-mb or 850-mb since ∇T is typically larger there as compared to higher aloft.

(\dot{Q}) Diabatic heating (Missing!!)

$\nabla^2 \dot{Q}$ Positive \rightarrow Ascent

$\nabla^2 \dot{Q}$ Negative \rightarrow Descent

Operational practice! Must be inferred by any information related to

\dot{Q} important over open ocean ~~with~~ with warm water

organized convection or potential driver thereof (satellite, radar, SSTs)

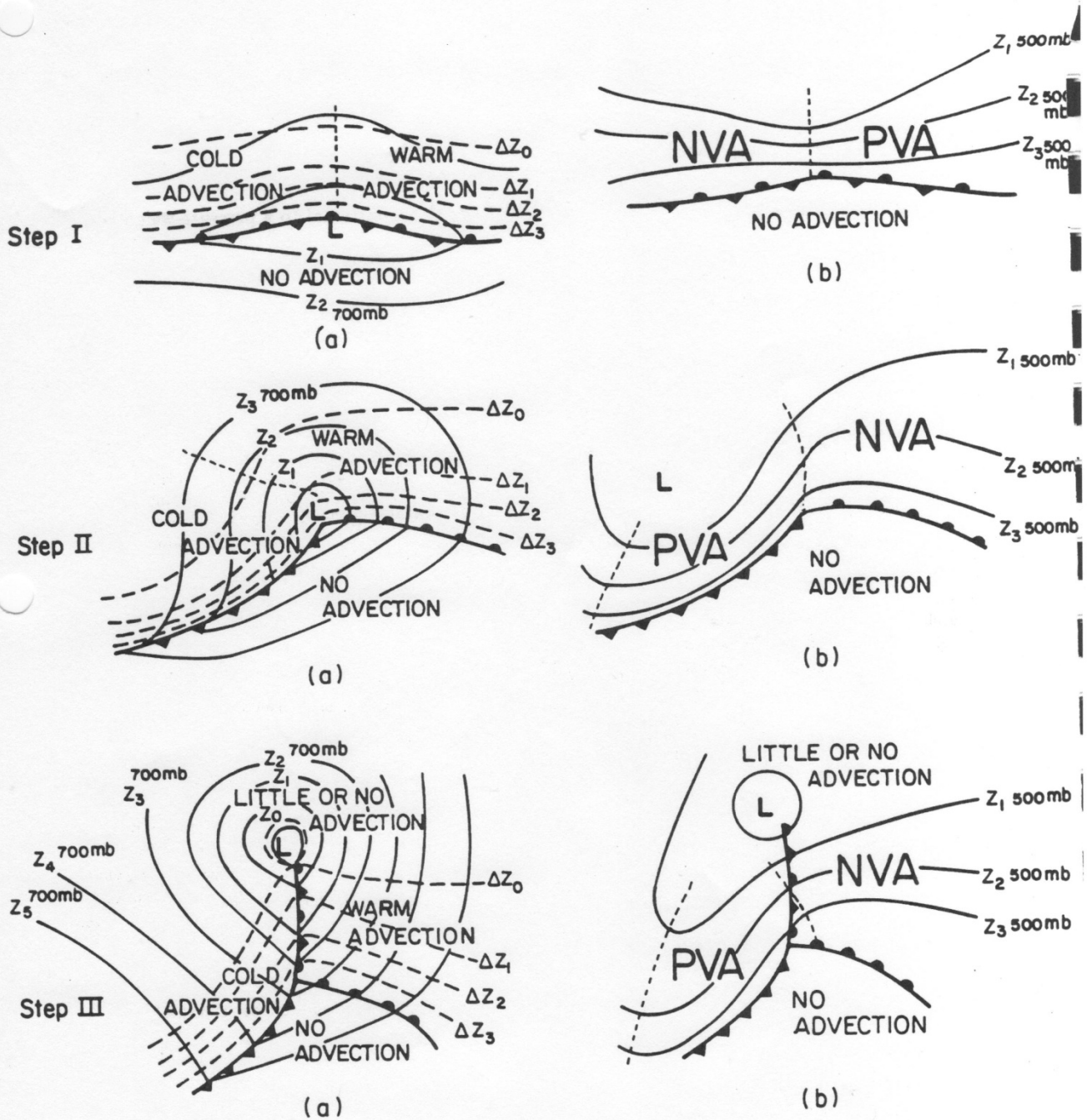


Figure 3.20: Schematic illustration of thickness advection and vorticity advection associated with extratropical cyclone development. The 700 mb height contours (solid lines), 1000-500 mb thickness contours (dashed lines), and surface frontal location are given in (a). The 500 mb height contours (solid lines) and surface frontal location are shown in (b).

Solving Q6

Can be done numerically by relaxation, a standard technique to solve an elliptic equation of the form $\nabla^2 \chi$ (Laplacian)
More in my modeling course...

Caveats to Q6

- Vertical motion is net result of all forcing terms. Terms may cancel each other out!!
- Always remember scaling assumptions! Will necessarily neglect any of the effects that lead to vertical motion on mesoscale.
- For above reason, Q6 vertical motion more reasonable in cool vs. warm season (where more convective)
- In practice, Q6 omega equation should be used to make qualitative diagnoses of vertical motion from upper-air data, that should conform to anything diagnosed in a numerical model.

Q-vectors

Motivation! We need a convenient way to diagnose QG vertical motion directly from wind and temperature fields on a Wp map.

Derivation

u-momentum equation (QG)

$$\frac{\partial u_g}{\partial t} + u_g \frac{\partial u_g}{\partial x} + v_g \frac{\partial u_g}{\partial y} - f v + \frac{\partial \Phi}{\partial x} = 0$$

$$v_{ag} + v_g = v \quad f v_g = \partial \Phi / \partial x$$

Yields:

$$\frac{\partial u_g}{\partial t} + \vec{v}_g \cdot \nabla u_g - f v_{ag} = 0$$

Take derivative wrt z and multiply by f .

Momentum result

$$\left(\frac{\partial}{\partial t} + \vec{v}_g \cdot \nabla \right) f \frac{\partial u_g}{\partial z} - f^2 \frac{\partial v_g}{\partial z} = -f \frac{\partial \vec{v}_g}{\partial z} \cdot \nabla u_g$$

RHS of equation contains thermal wind

$$-f \frac{\partial \vec{v}_g}{\partial z} \cdot \nabla u_g = \frac{-g}{\rho_0} (\hat{k} \times \nabla \theta) \cdot \nabla u_g$$

*equivalent to $\hat{k} \times \frac{\partial \vec{v}_g}{\partial z} \cdot \nabla u_g$

*see
aside.

ASIDE

RHS of equation contains thermal wind

$$-f \frac{\partial \vec{v}_g}{\partial z} \cdot \nabla u_g = -\frac{g}{\theta_0} (\hat{k} \times \nabla \theta) \cdot \nabla u_g$$

Expressed with θ here.

↓
equivalent to
 $\hat{k} \times \frac{\partial \vec{v}_g}{\partial y}$

Proof

$$\vec{v}_g = u_g \hat{i} + v_g \hat{j}$$

$$\nabla u_g = \hat{i} \frac{\partial u_g}{\partial x} + \hat{j} \frac{\partial u_g}{\partial y}$$

$$\nabla v_g = \hat{i} \frac{\partial v_g}{\partial x} + \hat{j} \frac{\partial v_g}{\partial y}$$

$$\hat{k} \times \frac{\partial \vec{v}_g}{\partial y} = \hat{k} \times \left(\hat{i} \frac{\partial v_g}{\partial y} + \hat{j} \frac{\partial u_g}{\partial y} \right)$$

$$\hat{k} \times \hat{i} = \hat{j} \quad \hat{k} \times \hat{j} = -\hat{i}$$

$$= \hat{j} \frac{\partial v_g}{\partial y} - \hat{i} \frac{\partial u_g}{\partial y}$$

since $\frac{\partial v_g}{\partial y} + \frac{\partial u_g}{\partial x} = 0$

$$= \hat{i} \frac{\partial u_g}{\partial x} + \hat{j} \frac{\partial u_g}{\partial y}$$

$$-\frac{g}{\theta_0} (\hat{k} \times \nabla \theta) \cdot (\hat{k} \times \frac{\partial \vec{v}_g}{\partial y}) = -\frac{g}{\theta_0} \frac{\partial \vec{v}_g}{\partial y} \cdot \nabla \theta$$

Final result for u-momentum

$$\left(\frac{\partial}{\partial t} + \vec{v}_g \cdot \nabla \right) f \frac{\partial u_g}{\partial z} - f^2 \frac{\partial v_g}{\partial z} = -\frac{g}{\theta_0} \frac{\partial \vec{v}_g}{\partial y} \cdot \nabla \theta$$

Thermodynamic equation (θ)

$$\frac{\partial \theta}{\partial t} + u_g \frac{\partial \theta}{\partial x} + v_g \frac{\partial \theta}{\partial y} + \frac{\theta_0}{g} N^2 w = 0$$

Boussinesq.
approx. applied.

$$N^2 = g \frac{d \ln \theta_0}{dz}$$

Multiply by g/θ_0 and take derivative wrt y

$$\frac{\partial}{\partial y} \left[\left(\frac{\partial}{\partial t} + \vec{v}_g \cdot \nabla \right) \frac{g}{\theta_0} \theta + N^2 w \right] = 0$$

Final result for thermodynamic

$$\left(\frac{\partial}{\partial t} + \vec{v}_g \cdot \nabla \right) \frac{g}{\theta_0} \frac{\partial \theta}{\partial y} + N^2 \frac{\partial w}{\partial y} = -\frac{g}{\theta_0} \frac{\partial \vec{v}_g}{\partial y} \cdot \nabla \theta$$

Add momentum and thermodynamic results . .

First terms in each equation cancel because of thermal wind relation

$$N^2 \frac{\partial w}{\partial y} - f^2 \frac{\partial v_{ag}}{\partial z} = -2 \frac{g}{\sigma_0} \frac{\partial \vec{v}_{ag}}{\partial y} \cdot \nabla \theta$$

Q-vector in y-direction

$$-\frac{g}{\sigma_0} \frac{\partial \vec{v}_{ag}}{\partial y} \cdot \nabla \theta \hat{j} = Q_y$$

Q-vector in x-direction (analogously)

$$-\frac{g}{\sigma_0} \frac{\partial \vec{v}_{ag}}{\partial x} \cdot \nabla \theta \hat{i} = Q_x$$

Total Q-vector

$$\vec{Q} = -\frac{g}{\sigma_0} \left(\frac{\partial \vec{v}_{ag}}{\partial x} \cdot \nabla \theta, \frac{\partial \vec{v}_{ag}}{\partial y} \cdot \nabla \theta \right) = (Q_x, Q_y)$$

Physical interpretation of Q-vector

Ageostrophic components of wind act to maintain thermal wind balance. An overturning circulation balances geostrophic advection of θ .

$$2Q_y = N^2 \frac{\partial w}{\partial y} - f^2 \frac{\partial v_{ag}}{\partial z} = -2 \frac{g}{\theta_0} \frac{\partial \vec{v}_{ag}}{\partial y} \cdot \nabla \theta$$

↑
↑
 Measure of overturning circulation Geostrophic advection of θ .

Divergence of Q-vector defines Q_6 .
omega equation

$$N^2 \nabla^2 w + f^2 \frac{\partial}{\partial z} \frac{\partial(pw)}{\partial z} = 2 \nabla \cdot \vec{Q}$$

In book: Magnitude given by

$$Q_1 = - \left[\frac{\partial u_{ag}}{\partial x} \frac{\partial \theta}{\partial x} + \frac{\partial v_{ag}}{\partial x} \frac{\partial \theta}{\partial y} \right]$$

$$Q_2 = - \left[\frac{\partial u_{ag}}{\partial y} \frac{\partial \theta}{\partial x} + \frac{\partial v_{ag}}{\partial y} \frac{\partial \theta}{\partial y} \right]$$

* Negative sign if use w as in book.

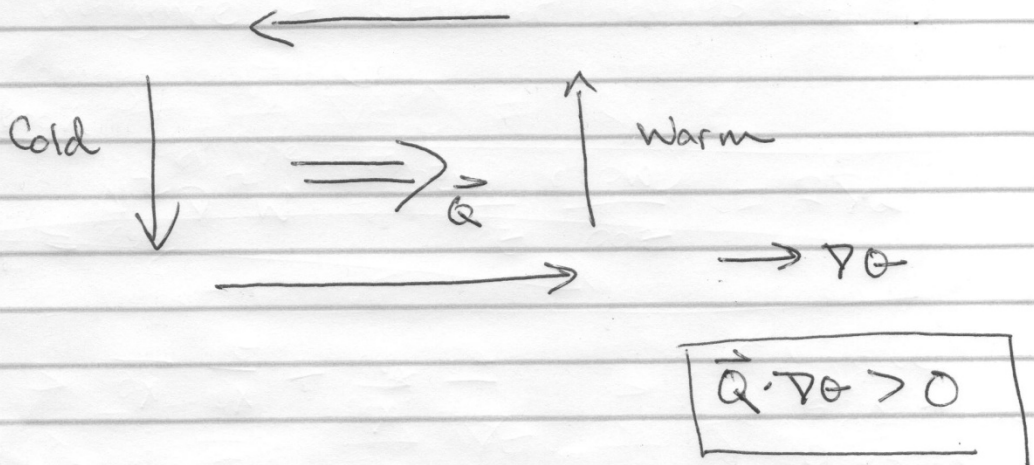
← How you can use to qualitatively diagnose Q_6 -vertical motion on Wp map. (Fig. 2.10)

$\nabla \vec{Q} = + \Rightarrow$ Convergence of Q
vectors
RISING AIR

$\nabla \vec{Q} = - \Rightarrow$ Divergence of Q
vectors
SINKING AIR

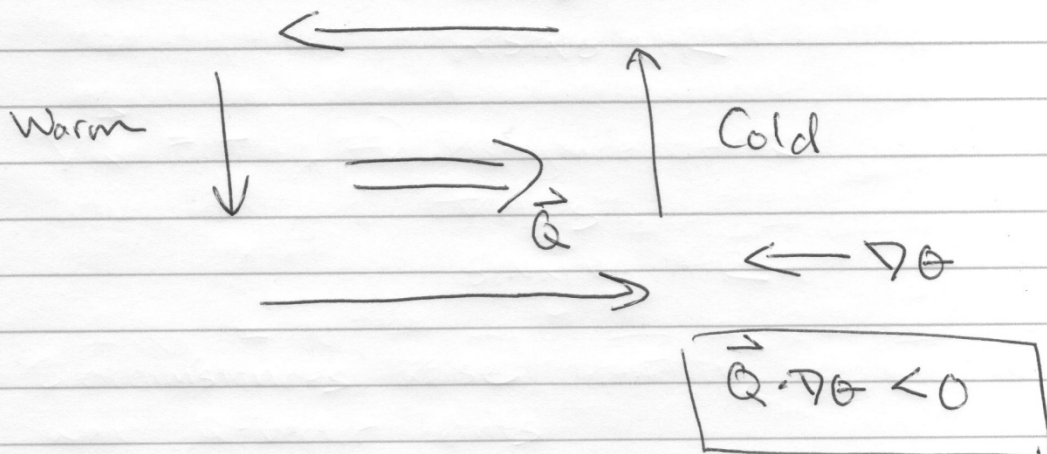
2 circumstances arise depending on which
way Q -vector points

Frontogenesis: Thermally direct



Ageostrophic circulation tries to
weaken $\nabla \theta$

Frontolysis! Thermally-indirect



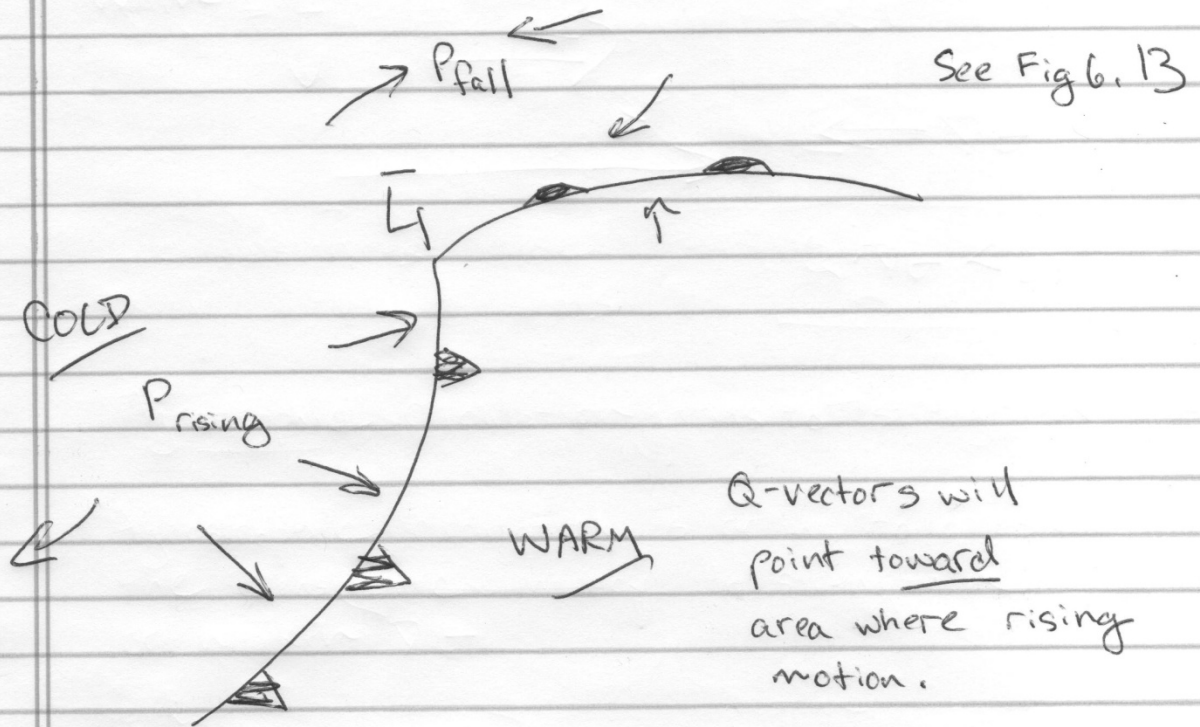
Ageostrophic circulation tries to strengthen $\nabla\theta$

Ageostrophic circulation is acting to oppose the geostrophic tendency to strengthen or weaken $\nabla\theta$.

In the case of frontogenesis, intensifying gradients mean that ageostrophic circulation is not strong enough to overcome the effects of the concentration of $\nabla\theta$ by advective terms.

Aside! Strength of fronts will be inherently underestimated by $\alpha\theta$ -theory, because effects of advection by v_{ag} are not accounted for.

Q-vectors in relation to mid-latitude cyclone



Advantages of Q-vector vs. $\Omega\delta - \omega$:

- 1) No cancellation problem (if tendencies are opposing)
- 2) Q-vectors computed at single level (no differential aspect)
- 3) Patterns of divergence given concentrated areas with synoptic-scale vertical motion likely to occur. So better proxy for any model computed ω .